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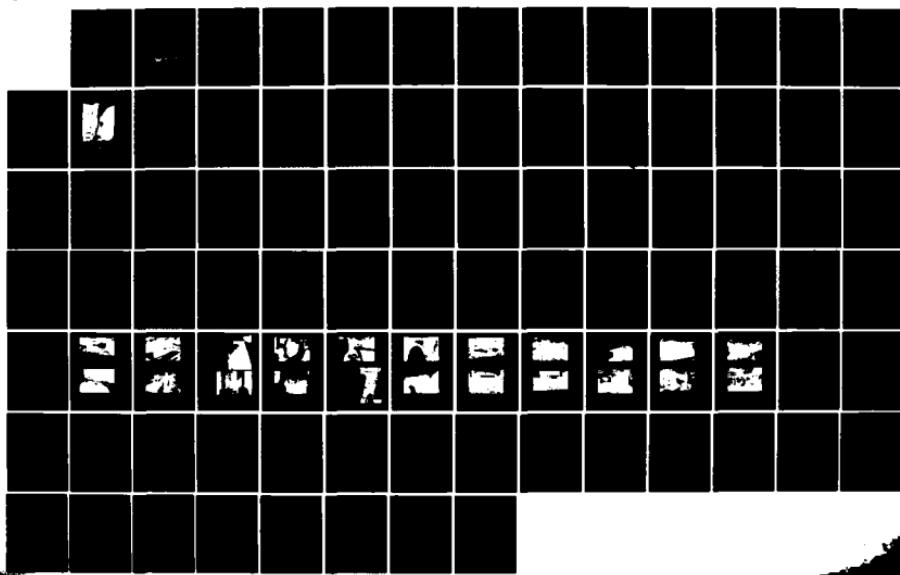
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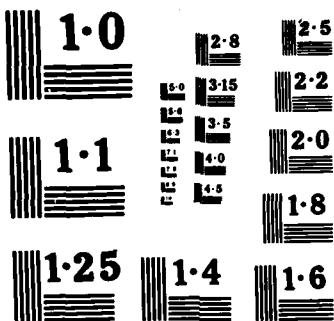
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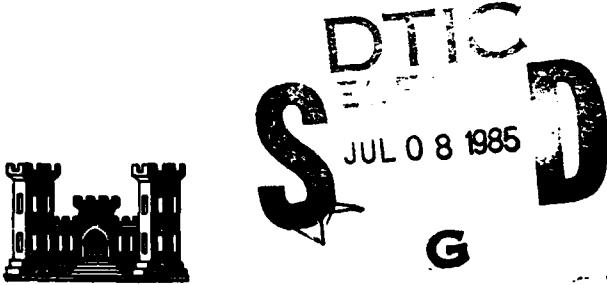
MERRIMACK RIVER BASIN  
HARRISVILLE, NEW HAMPSHIRE

**HARRISVILLE POND DAM  
NH 00065**

NHWRB 109.08

**PHASE I INSPECTION REPORT  
NATIONAL DAM INSPECTION PROGRAM**

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**DEPARTMENT OF THE ARMY  
NEW ENGLAND DIVISION, CORPS OF ENGINEERS  
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MAY 1979

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The dam is a dry rubble masonry and earth dam. The dam has a maximum height of 21 ft. and is about 75 ft. long. The dam is judged to be in fair condition. It is intermediate in size with a high hazard potential. Modification is necessary to improve the hydraulic and hydrological condition of the dam.		

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424 TRAPELO ROAD  
WALTHAM, MASSACHUSETTS 02154

REPLY TO  
ATTENTION OF:  
NEDED-E

SEP 6 1973

Honorable Hugh J. Gallen  
Governor of the State of New Hampshire  
State House  
Concord, New Hampshire 03301

Dear Governor Gallen:

Inclosed is a copy of the Harrisville Pond Dam Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. The report is based upon a visual inspection, a review of past performance, and a preliminary hydrological analysis. A brief assessment is included at the beginning of the report.

The preliminary hydrologic analysis has indicated that the spillway capacity for the Harrisville Pond Dam would likely be exceeded by floods greater than 2.5 percent of the Probable Maximum Flood (PMF), the test flood for spillway adequacy. Our screening criteria specifies that a dam of this class which does not have sufficient spillway capacity to discharge fifty (50) percent of the PMF, should be adjudged as having a seriously inadequate spillway and the dam assessed as unsafe, non-emergency, until more detailed studies prove otherwise or corrective measures are completed.

The term "unsafe" applied to a dam because of an inadequate spillway does not indicate the same degree of emergency as that term would if applied because of structural deficiency. It does indicate, however, that a severe storm may cause overtopping and possible failure of the dam, with significant damage and potential loss of life downstream.

It is recommended that within twelve months from the date of this report the owner of the dam engage the services of a professional or consulting engineer to determine by more sophisticated methods and procedures the magnitude of the spillway deficiency. Based on this determination, appropriate remedial mitigating measures should be designed and completed within 24 months of this date of notification. In the interim a detailed emergency operation plan and warning system should be promptly developed. During periods of unusually heavy precipitation, round-the-clock surveillance should be provided.

A/

Py	Disturbance	Assessment	Specs	Accommodation for
1	2	3	4	NTS GRA&I DTIC TAB Unneeded Justification Refrigerator X

NEDED-E

Honorable Hugh J. Gallen

I have approved the report and support the findings and recommendations described in Section 7, with qualifications as noted above. I request that you keep me informed of the actions taken to implement these recommendations since this follow-up is an important part of the non-Federal Dam Inspection Program.

A copy of this report has been forwarded to Water Resources Board, the cooperating agency for the State of New Hampshire. This report has also been furnished to the owner of the project, Mr. John J. Colony, Jr., c/o Harrisville Designs, Harrisville, New Hampshire 03450.

Copies of this report will be made available to the public, upon request to this office, under the Freedom of Information Act, thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Water Resources Board for the cooperation extended in carrying out this program.

Sincerely,

*Max B. Scheider*  
MAX B. SCHEIDER  
Colonel, Corps of Engineers  
Division Engineer

HARRISVILLE POND DAM

NH 00065

NHWRB 109.08

MERRIMACK RIVER BASIN  
HARRISVILLE, NEW HAMPSHIRE

PHASE I INSPECTION REPORT  
NATIONAL DAM INSPECTION PROGRAM

NATIONAL DAM INSPECTION PROGRAM  
PHASE I INSPECTION REPORT

Identification No.: NH 00065  
Name of Dam: Harrisville Pond Dam  
Town: Harrisville  
County and State: Cheshire, New Hampshire  
Stream: Nubanusit Brook  
Date of Inspection: May 22, 1978

Brief Assessment

Harrisville Pond Dam is a dry rubble masonry and earth dam which was constructed around 1886. The dam has a maximum height of 21 feet and is approximately 75 feet long. It is serving as the foundation of the north wall of a 2-story mill building. The spillway, located in the western end, is 3 feet 7 inches wide with a 2.5-foot high opening in the wall.

Based on the visual inspection, available records, and past operational performance, the dam is judged to be in fair condition. Water was observed seeping out of the downstream face of the dam and at the gate structure. Settlement was noted east of the gate structure. Continuance of this classification depends on proper operations and maintenance of the dam.

This dam falls under the category of high hazard potential, and it is intermediate in size. The test flood peak inflow is equal to the Probable Maximum Flood, 16,500 cfs, and the test flood peak outflow is 14,289 cfs. Hydraulic analysis indicates that the maximum surcharge pool elevation is 1329.4, approximately 11.4 feet above the spillway crest. The spillway in the body of the dam together with the waste sluice will pass approximately 2.5% of the test flood peak outflow without overtopping the county road above the by pass culvert. Therefore, the spillway capacity is inadequate. The test flood would overtop the county road by 8.9 feet.

As stated in Section 7, within 1 year after receipt of this Phase I report, the owner, Mr. John J. Colony, Jr., should retain the services of a competent engineer and implement the results of his evaluation of the following:

1. The modification necessary to improve the hydraulic and hydrologic condition of the dam.

2. The extent of submergence in Eastview and Harrisville in the event of failure of this dam.

The following operating and maintenance measures, as stated in Section 7.3, should also be implemented:

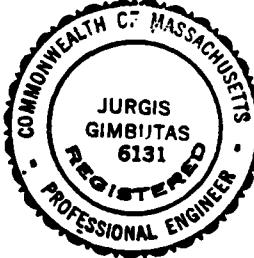
1. Leaks through the face of the dam should be monitored regularly until such time it can be repaired.
2. Reestablish the proper grade of the settled area east of the gate structure.
3. An operating and maintenance manual for the project should be prepared.
4. A program of technical annual periodic inspection of the project features should be prepared and initiated. This program should assure that all features of the foundation of the mill building within the discharge channel are continually maintained.
5. Surveillance and a warning system should be developed for periods of unusually heavy rains and runoff.

FAY, SPOFFORD & THORNDIKE, INC.

By

*Jurgis Gimbutas*  
Jurgis Gimbutas, P.E.  
Project Engineer

*Richard W. Albrecht*  
Richard W. Albrecht, P.E.  
Vice President



This Phase I Inspection Report on Harrisville Pond Dam has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the Recommended Guidelines for Safety Inspection of Dams, and with good engineering judgment and practice, and is hereby submitted for approval.

Charles G. Tiersch

CHARLES G. TIERSCH, Chairman  
Chief, Foundation and Materials Branch  
Engineering Division

Fred J. Ravers Jr.

FRED J. RAVENS, Jr., Member  
Chief, Design Branch  
Engineering Division

Saul Cooper

SAUL COOPER, Member  
Chief, Water Control Branch  
Engineering Division

APPROVAL RECOMMENDED:

Joe B. Fryar

JOE B. FRYAR  
Chief, Engineering Division

## PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonable possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

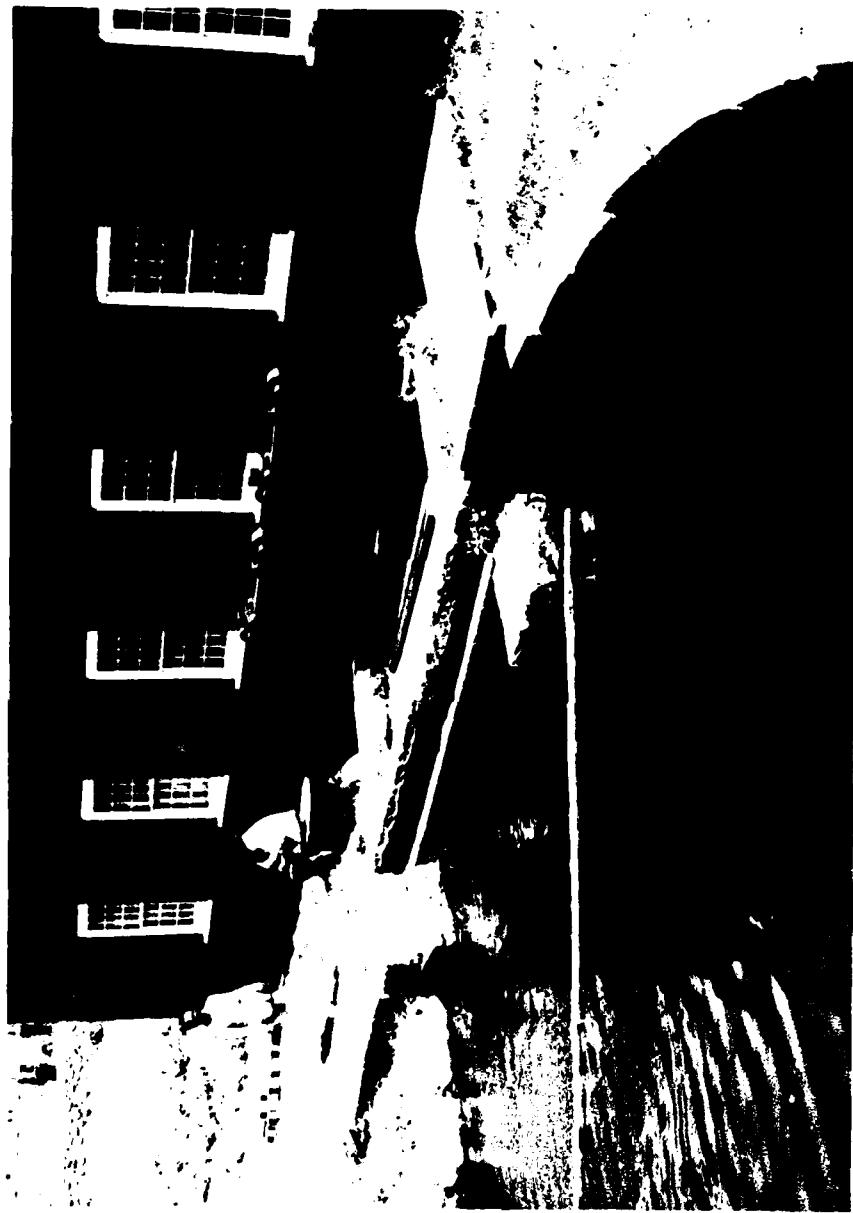
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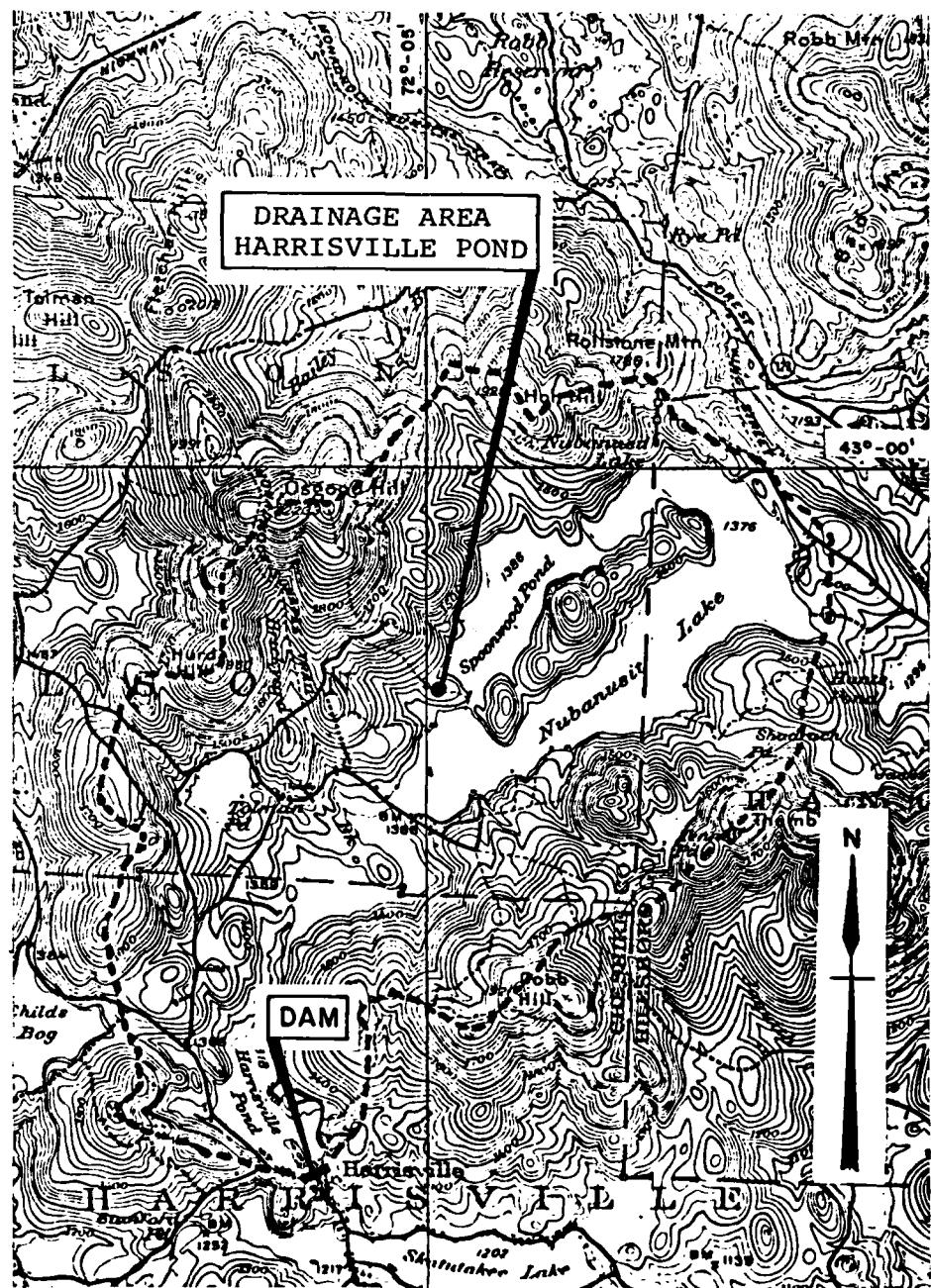
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OVERVIEW PHOTOGRAPH



HARRISVILLE DAM, LOOKING SOUTHEAST  
Negative No. I-13



UNITED STATES  
DEPARTMENT OF INTERIOR  
GEOLOGICAL SURVEY

NEW HAMPSHIRE  
MONADNOCK QUADRANGLE 1949  
AMS 6569 I-SERIES V712

LOVELL MOUNTAIN QUADRANGLE 1957  
AMS 6570 II-SERIES V712

## HARRISVILLE POND DAM

### SECTION 1 - PROJECT INFORMATION

#### 1.1 General

##### a. Authority

Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Fay, Spofford & Thorndike, Inc., Engineers, have been retained by the New England Division to inspect and report on selected dams in the State of New Hampshire. Authorization and notice to proceed was issued to Fay, Spofford & Thorndike, Inc., under a letter of May 3, 1978, from Mr. Ralph T. Garver, Colonel, Corps of Engineers. Contract No. DACW 33-78-C-0308 has been assigned by the Corps of Engineers for this work.

##### b. Purpose:

- (1) Perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
- (2) Encourage and prepare the States to initiate quickly effective dam safety programs for non-Federal dams.
- (3) To update, verify, and complete the National Inventory of Dams.

#### 1.2 Description of Project

##### a. Location

Harrisville Pond Dam, locally called the "Upper Pond Dam," is located near the southwest bay of Harrisville Pond, which is a natural pond. It is located in the southwestern part of New Hampshire in the center of the Town of Harrisville, near the Post Office, and about 10 miles east of Keene. Tolman Pond, Brick Yard Brook, and two conservation reservoirs, namely, Spoonwood Lake and Nubanusit Lake, drain into Harrisville Pond. Harrisville Pond drains into Skatutakee Lake,

which in turn drains into Nubanusit Brook, Contoocook River, and finally into the Merrimack River.

b. Description of Dam

The dam, built in 1886, is of stone masonry, 21 feet high, 75 feet long, and approximately 14 feet wide. The spillway, which is located in the western end, is 3 feet 7 inches wide and is approximately 2.5 feet below the top of the dam. Approximately in the center of the dam, there are four gates, 2 feet by 3 feet each, and all are operated by rack and pinion. Two gates open into a penstock, the other two open into a 6-foot high, 4-foot wide outlet conduit. The penstock pipe, 4 feet in diameter, is not in use (Photographs No. 7, 8, 9, and 10, Appendix C).

A two-story mill building was built adjacent to this dam with the dam serving as a foundation for the north wall. The abutments of this masonry dam are of earth, granite faced (Photographs No. 1 and 2, Appendix C).

The intake channel consists of two small ponds connected by two culverts under roads crossing parallel to the dam. The first bridge, which is near the dam, has a 14.5-foot by 10-foot opening, with a 4-foot freeboard. The second bridge, which is near Harrisville Pond, has an 11-foot by 7-foot opening with a 1.5-foot freeboard (Photographs No. 17 and 18, Appendix C).

At the southeast bay of the Harrisville Pond, approximately 400 feet north of the intake channel, there is an rudimentary type weir and a culvert under a road. This weir is about 16 feet long, curved in plan, and has approximately a 1-foot drop. The discharge from the 4-foot culvert reenters the outlet channel below the toy shop (Photographs No. 19, 20, 21, and 22, Appendix C).

c. Size Classification

The storage capacity at the spillway crest is 2,000 acre-feet, which falls in the range  $\geq 1,000$  and  $< 50,000$  acre-feet. Therefore, the dam is classified as intermediate in size.

d. Hazard Classification

In the event of failure of this dam, the lower Skatutakee Dam might fail by domino effect and the village of Eastview, which is at a distance of about 2 1/2 miles downstream of Harrisville Pond Dam, will be in danger of being flooded. The mill building, toy shop, and the Filtrine Manufacturing Mills which are located downstream would be

damaged with eventual loss of the lives of the people in these structures. It is estimated that in the event of failure of this dam, loss of more than a few lives and excessive property damage could occur. Therefore, this dam falls in the category of high hazard potential.

e. Ownership

The oldest available inventory, dated 1925, gives the Cheshire Mills as the owner. The earliest available letter, signed by the present owner, Mr. John J. Colony, Jr., of the Cheshire Woolen Co. of Harrisville, New Hampshire, telephone 603-827-3402, was dated in 1942.

f. Operator

The owner: Mr. John J. Colony, Jr., (see Section 1.2.e.).

g. Purpose of the Dam

The pond behind the dam had been supplying water power for the Cheshire Woolens Co. mills until 1942, when electrically driven machinery was installed. However, the Filtrine Manufacturing Co. mills still depend on the water coming downstream. They need the water power to operate the hydro-electric turbine of the Northern Water Power Co. and to supply water for the fire protection system of the mill. The Northern Water Power Co. is a tenant of the Filtrine Manufacturing Co.

Currently, Harrisville Pond is being used primarily for recreational purposes.

h. Design and Construction History

There is no available data on the original design and construction of this dam. This dam was probably constructed around 1886, and no records of alterations are available. According to inspection reports and questionnaires, dated 1937, the dam was in good repair with the gates in operable condition, as they presently exist.

In 1974, some leaks were noticed near the penstock which was not and presently is not in use. In 1976, leakage through the stonework of the dam was observed on the downstream side. The water level was drawn down below the normal full pond level and the voids located and repaired. These voids occurred in the top few feet of the fill between the intake channel stonework and the dam stonework. Some settlement of backfill is visible in a small area on the east side of the intake structure.

In May, 1978, the old wooden planking over the intake structure was replaced by new flooring.

i. Normal Operation Procedures

The responsibility of operating the reservoir rests with the owner, Mr. John J. Colony, Jr. As the penstock was abandoned in 1942, and the spillway is ungated, the only control available is by two gates which are operable by rack and pinion. These gates open into the 6-foot high, 4-foot wide outlet conduit. During storms in the spring, both gates are kept open. If the water level in Harrisville Pond rises above a certain level, which level is not known from the project records, the water from the pond will pass over the rudimentary type weir at the southeast bay of Harrisville Pond.

1.3 Pertinent Data

a. Drainage Area

Harrisville Pond, as shown on the U.S.G.S. map, is located on Nubanusit Brook Watershed. This reservoir is a natural one and it has a drainage area of 10 square miles. The drainage area is best characterized as heavily wooded and its topography is undulated and rolling.

b. Discharge at Dam Site

(1) Outlet works (conduits) are permanently closed. The penstock is 4 feet in diameter and has an invert elevation of 1305.3 (estimated). The sluice opening is approximately 6 feet by 4 feet with an invert elevation of 1305.3 (estimated).

397.0 cfs through sluice at Elevation 1329.4.

(2) The maximum known flood at the dam site is the flood of September 21-24, 1938, magnitude not recorded.

(3) Ungated spillway capacity at the top of dam - not applicable.

(4) Ungated spillway capacity at test flood maximum pool.

123 cfs at Elevation 1329.4.

(5) Flow through 4-inch pipe culvert test flood maximum pool.

290.0 cfs at Elevation 1329.4.

c. Elevation (Feet above MSL)

(1) The top of the dam serves as a foundation of the north wall of a two-story mill building, which is adjacent to this dam.

(2) Test flood maximum pool elevation is 1329.40.

(3) The full flood control pool - unknown.

(4) The recreation pool (assumed from USGS data) is 1318.

(5) The spillway crest (assumed from USGS data) is 1318.

(6) The stream bed at the centerline of the dam is 1297 (estimated).

(7) The maximum tail water is 1304 (estimated).

d. Reservoir

(1) The length of the maximum pool is 7,500 feet (estimated).

(2) The length of recreation pool is 5,000 feet (estimated).

(3) The length of flood control pool is 6,000 feet (estimated).

e. Storage (Acre-Feet)

(1) Top of dam - not applicable.

(2) Test flood maximum pool elevation - 5,397 acre-feet.

(3) The flood control pool - unknown.

(4) The recreation pool - 2,000 acre-feet.

(5) Spillway crest - 2,000 acre-feet.

f. Reservoir Surface (Acres)

- (1) The top of the dam - not applicable.
- (2) Test flood maximum pool elevation - 358 acres.
- (3) The flood control pool - unknown.
- (4) The recreation pool - 119 acres.
- (5) The spillway crest - 119 acres.

g. Dam

(1) Type	Dry rubble masonry and earth fill
(2) Length	75 feet
(3) Height	21 feet
(4) Top width	Approximately 14 feet
(5) Side slopes	
(a) Upstream	Vertical
(b) Downstream	Vertical
(6) Zoning	Not applicable
(7) Impervious core	Not applicable
(8) Cutoff	None
(9) Grout curtain	None
h. Spillway	
(1) Type	Ungated weir
(2) Length of weir	3 feet 7 inches
(3) Crest elevation	1318 (estimated)
(4) Gates	None

(5) U/S channel

Pond

i. Regulating Outlets

The regulating outlet consists of an approximately 4-foot wide, 6-foot high waste sluice opening at the downstream face and a 4-foot diameter penstock. These are adjacent to each other. The flow through each outlet is controlled by two manually operated gates. Each gate is approximately 2 feet by 3 feet in dimension.

(1) Invert	Elevation 1305.3
(2) Size	48-inch diameter
(3) Description	Steel penstock
(4) Control mechanism	Two gates, manually operated
(5) Other	
(a) Invert	1305 (estimated)
(b) Size	Width - approximately 4 feet Depth - approximately 6 feet Length - approximately 14 feet
(c) Description	Stone masonry waste sluice opening
(d) Control mechanism	Two gates, manually operated

## SECTION 2 - ENGINEERING DATA

### 2.1 Design

No original design data was disclosed for Harrisville Pond Dam.

### 2.2 Construction

No engineering data are available on the construction of this dam.

### 2.3 Operation

No engineering operational data were disclosed.

For information pertaining to the history of previous failures or deficiencies, refer to Section 1. For operational porocedures refer to Sections 1.2.i and 4.

### 2.4 Evaluation

#### a. Availability

Pertinent structural, geotechnical, hydrologic, and hydraulic data, which formed the basis of the design of the dam, are available on a very limited basis. The hydraulic and hydrologic determinations for design, as collected from project records, were obtained by rule of thumb techniques.

#### b. Adequacy

Sufficient engineering data are available for a Phase I inspection.

#### c. Validity

The available engineering data is considered valid on the basis of the results of the visual inspection.

### SECTION 3 - VISUAL INSPECTION

#### 3.1 Findings

The Phase I inspection of the Harrisville Pond Dam was performed on May 22, 1978. A copy of the inspection check list is included in Appendix A.

##### a. General

In general, the soil and rock features are in good condition. The only concrete observed was the topping placed on the apron walls.

##### b. Dam

No evidence of vertical or horizontal misalignment was observed. There is no indication of sloughing, bulging, or movement of the slopes, nor is there evidence of piping.

Water was observed seeping out of the downstream face of the dam on either side of the gates.

Within approximately 4 feet east of the gate structure adjacent to the mill building, the top portion of the dam has settled to a maximum depth of 4 feet. At the time of the inspection, water, minor in nature, was flowing in the vicinity of the gate structure into this depression. There is no apparent distress of the wall of the mill as a result of this settlement.

##### c. Appurtenant Structures

At the time of our inspection, all four sluice gates were closed. Water was observed flowing through the penstock, which indicates that the two gates opening into the penstock are leaking. The east gate, which controls the flow through the waste sluice opening, was leaking. The gates and their lifting mechanism are in operable condition. The approach to and the accessibility to the operating platform is well maintained.

The 48-inch steel penstock is in poor condition. A hole was observed in the top of the penstock near the dam. Leakage was also observed at the bottom of the penstock.

On the upstream side of the dam, the masonry is backfilled, except for the intake structure which is under water. Therefore, the

upstream face of the masonry could not be seen. Inside of the mill building, the exposed face of rubble masonry appears to be sound.

The rudimentary type weir at the southeast bay of Harrisville Pond, and the 4 foot diameter circular pipe under the country road, approximately 400 feet east of the dam, are in fair condition. Observation indicates that this weir is primitively constructed with miscellaneous materials such as loose stone and wood. The approach and discharge channel and side slopes were observed to be in good condition.

The superstructure of both concrete bridges over the intake channel appears to be in good condition. The concrete abutments have deteriorated at the water level, exposing the aggregates.

d. Reservoir Area

Harrisville Pond is located on the Nubanusit Brook watershed. The surface area of the pond is 119 acres. The reservoir area is accessible and its shoreline is heavily wooded.

e. Downstream Channel

The initial 45 feet of this channel was found to be the basement of the mill building, the next 60 feet, a stone-lined channel, and the next 20 feet, an opening in the foundation of the toy shop. Columns supporting the mill floor were observed in the channel. It appears that these columns were either repaired or replaced recently. Brick work in both the mill building and the toy shop appears to be in good condition. Debris was observed in the basement of the mill building. The quantity of debris will not impede the flow in the channel.

The downstream channel and side slopes were observed to be in good condition.

3.2 Evaluation

The observed condition of the dam is fair. The potential problems observed during the visual inspection are listed as follows:

- (1) Leaks through the face of the dam and at the gate structure.
- (2) Settlement east of the gate structure.
- (3) Potential for overtopping of the country road at the bypass culvert.

(4) Potential for floods to rise against the wall of the building above the dam.

## SECTION 4 - OPERATIONAL PROCEDURES

### 4.1 Procedures

Mr. John J. Colony, Jr. has operated Harrisville Pond Dam since about 1942. The Pond level is maintained by a broad-crested spillway located at the western end of the dam. The flow is controlled by stop logs manually operated. The Pond can be lowered by the opening of two gates, which are operable by rack and pinion.

### 4.2 Maintenance of Dam

The maintenance of Harrisville Pond Dam is the responsibility of Mr. John J. Colony, Jr., of the Cheshire Woolen Co. of Harrisville.

### 4.3 Maintenance of Operating Facilities

No written maintenance procedures were disclosed for Harrisville Pond Dam. As the penstock is not used, the question of its operation does not arise. The possibility and/or permissibility of the gate operations controlling the flow through the sluice opening is not known. In view of the location of the foundation of the building, there is a possibility of the building being undermined if the gates are left open. The approach to and the accessibility to the operating platform is well maintained. Maintenance of the facilities for operating stop logs across the broad-crested spillway in the body of dam is satisfactory.

### 4.4 Description of any Warning System in Effect

A flood warning system is non-existent.

### 4.5 Evaluation

The current operation and maintenance procedure for Harrisville Pond Dam are inadequate to ensure that all problems can be remedied within a reasonable period of time.

## SECTION 5 - HYDRAULIC/HYDROLOGIC

### 5.1 Evaluation of Features

#### a. Design Data

- (1) This dam falls under the category of high hazard potential and it is intermediate in size. Using the "Recommended Guidelines for Safety Inspection of Dams", the recommended spillway test flood peak inflow is equal to the Probable Maximum flood. The spillway test flood inflow hydrograph, estimated, is furnished in Appendix D. The spillway test flood peak inflow is 16,500 cfs.
- (2) The estimated peak outflow corresponding to the spillway test flood inflow is about 14,289 cfs. Refer to Appendix D for further details.
- (3) The pond storage capacity versus the elevation, an estimated capacity curve is furnished in Appendix D.
- (4) The composite discharge rating curve for the spillway, waste sluice and the country roadway above the 4 foot diameter culvert pipe is included in Appendix D.
- (5) The hydrologic map of the watershed above the dam site, including reservoir area, water course and principal stream flow, is included in Appendix D.

#### b. Experience Data

With the exception of sketchy information, past flood details are not available for Harrisville Pond Dam. Precipitation records for the area are available. It is noted that significant amounts of rainfall up to 12.43 inches, which was more than 3.5 times the monthly average rainfall, occurred in the month of September, 1938. The flood of September 21-24, 1938, is considered to be the maximum flood that has occurred. On the basis of regional frequency studies, the flood of 1938, corresponds to a 100-year flood.

All floods in the past were handled by opening the gates and using the culvert at the southeast bay of the lake.

### c. Visual Observations

The valley cross section immediately below the dam is not sufficiently wide to convey the peak outflow from the reservoir. This cross section is approximately 8 feet by 8 feet.

Harrisville Pond Dam is provided with a rudimentary type weir, which leads into a 4-foot diameter circular pipe under a country road. The invert of the culvert pipe in relation to the crest elevation of the spillway in the body of the dam is not determinable without additional data.

### d. Overtopping Potential

The dam is unusual since it forms part of the foundation of a mill building. The question of overtopping does not arise in the case of this dam. The length of the spillway is too small to handle the spillway test flood peak inflow that might result from 10 square miles of the drainage area of Harrisville Pond. Due to the unavailability of information, it is assumed that as soon as the water surface in the pond reaches Elevation 1320.5 there will be an overflow over the country road. To develop the composite discharge rating curve, flow through the waste sluice, spillway, and over the country road are only considered. It is also assumed that flow over the roadway would occur over an effective length of 200 feet. Based on these assumptions, an approximate composite rating curve for the spillway, the waste sluice, and the overflow over the roadway has been estimated and is furnished in Appendix D. The maximum pool elevation corresponding to the spillway test flood peak outflow is approximately 1329.4. The maximum surcharge height over the crest of the spillway is about 11.4 feet.

## SECTION 6 - STRUCTURAL STABILITY

### 6.1 Evaluation of Structural Stability

#### a. Visual Observations

The upstream slope could not be seen due to the fact that it was under water. The slopes do not show any erosion or weak areas. The visual inspection revealed the following evidence of possible stability problems:

- (1) Leaks through the face of the dam and at the gate structure.
- (2) Settlement east of the gate structure.

Visual inspection of the stone masonry did not reveal any evidence of instability.

#### b. Design and Construction Data

There are rough sketches in the inspection report dated 1937, but there are no structural computations. There are no other design and construction data available.

#### c. Operating Records

Except for memorandums and correspondence listed in Appendix B, other operating records are not available at the office of the New Hampshire Water Resources Board.

#### d. Post-Construction Changes

None recorded.

#### e. Seismic Stability

This dam is located in Seismic Zone 2 and in accordance with recommended Phase I guidelines does not warrant seismic analyses.

## SECTION 7 - ASSESSMENT, RECOMMENDATIONS & REMEDIAL MEASURES

### 7.1 Dam Assessment

#### a. Condition

Based on visual inspection, available records and past operational performance, the dam is judged to be in fair condition.

#### b. Adequacy of Information

An adequate assessment of the dam consistent with the scope of a Phase I investigation has been made based upon the visual inspection and available information.

#### c. Urgency

All recommendations and remedial measures enumerated below should be implemented within 1 year of receipt of this Phase I report by the owner.

#### d. Need for Additional Investigation

The information available from the visual inspection is adequate to identify the potential problem of overtopping. This problem will require the attention of a competent engineer who will have to make additional engineering studies to design or specify remedial measures to rectify the problem.

### 7.2 Recommendations

It is recommended that the owner retain the services of a competent engineer to do the following:

- (1) In view of the inadequate spillway capacity, it is considered advisable to conduct detailed studies. These studies should evaluate the possible extent of damage in Harrisville and Eastview in the event of failure of this dam and the downstream Skatutakee Dam by domino effect.
- (2) A study should be made to determine the modifications necessary to the rudimentary type weir and the culvert under the country road and its downstream channel to accommodate flood condition. Suggested modifications are lowering and increasing the size of the culvert, and enlarging the downstream channel to accommodate flood conditions. It should also include the feasibility of extending the discharge

channel of the overflow weir beyond the lower dam. During extreme flood events and spring runoff, this channel extension would be used and for the normal flow, the existing channel would be used.

#### 7.3 Remedial Measures

It is considered important that the following operating and maintenance procedures be attended to as early as practical:

- a. Leaks through the face of the dam should be monitored regularly until such time they can be repaired.
- b. Proper grade of the settlement area east of the gate structure should be reestablished.
- c. An operating and maintenance manual for the project should be prepared.
- d. A program of technical annual periodic inspection of the project features should be prepared and initiated. This program should assure that all features of the foundation of the mill building within the discharge channel are continually maintained.
- e. Because the dam is located upstream of a populated area, round-the-clock surveillance should be provided during periods of high precipitation.
- f. The owner should develop a formal warning system. An operational procedure to follow in event of an emergency should also be adopted.

#### 7.4 Alternatives

Until the hydraulic and hydrologic condition of this dam is improved, the pond should be operated at a lower level to provide more storage during extreme flood events and spring runoff.

**APPENDIX A**  
**VISUAL INSPECTION CHECK LISTS**

APPENDIX A

VISUAL INSPECTION CHECK LIST  
PARTY ORGANIZATION

PROJECT Harrisville Pond Dam DATE May 22, 1978  
TIME 930 - 1400  
WEATHER Sunny  
W. S. ELEV. 1318.7 U.S. \_\_\_\_\_ DN.S.

PARTY:

1. <u>Jurgis Gimbutas, P.E.</u>	<u>Team Captain - Structural and Concrete</u>
2. <u>Harvey H. Stoller, P.E.</u>	<u>Soils, Geology and Foundations</u>
3. <u>V. Rao Maddineni, P.E.</u>	<u>Hydraulics and Hydrology</u>
4. _____	_____
5. _____	_____

PROJECT FEATURE	INSPECTED BY	REMARKS
1. <u>Dam Embankments</u>	<u>H. H. Stoller</u>	<u>Fair</u>
2. <u>Penstock</u> <u>Outlet Works -</u>	<u>J. Gimbutas</u>	<u>Poor</u>
3. <u>Waste Sluice Opening</u>	<u>J. Gimbutas</u>	<u>Fair</u>
4. <u>Spillway Weir</u> <u>Approach and</u>	<u>J. Gimbutas</u>	<u>Good</u>
5. <u>Discharge Channels</u> <u>Rudimentary</u>	<u>H. H. Stoller</u>	<u>Good</u>
6. <u>Type Weir</u> <u>Approach and</u>	<u>V. R. Maddineni</u>	<u>Fair</u>
7. <u>Discharge Channels</u> <u>Pond and Downstream</u>	<u>H. H. Stoller</u>	<u>Good</u>
8. <u>Channel</u>	<u>V. R. Maddineni</u>	<u>Good</u>

**PERIODIC INSPECTION CHECK LIST**

PROJECT Harrisville Pond Dam

DATE May 22, 1978

PROJECT FEATURE Dam Embankment

NAME Henry H. Miller

DISCIPLINE Soils & Foundation

PROJECT FEATURE \_\_\_\_\_

NAME \_\_\_\_\_

DISCIPLINE \_\_\_\_\_

DISCIPLINE \_\_\_\_\_

NAME \_\_\_\_\_

AREA EVALUATED CONDITION

DAM EMBANKMENT

Crest Elevation	1320.5 (Estimated)
Current Pool Elevation	1318.7 (Estimated)
Maximum Impoundment to Date	Unknown
Surface Cracks	None observed
Pavement Condition	None
Movement or Settlement of Crest	East side of gate structure (see narrative)
Lateral Movement	None observed
Vertical Alignment	No visual vertical misalignment observed
Horizontal Alignment	No visual horizontal misalignment observed
Condition at Abutment and at Concrete Structures	No concrete structures

PERIODIC INSPECTION CHECK LIST

PROJECT Harrisville Pond Dam DATE May 22, 1978

PROJECT FEATURE Dam Embankment

DISCIPLINE Soils & Foundation NAME 34-114 J.L.C.

PROJECT FEATURE \_\_\_\_\_

DISCIPLINE \_\_\_\_\_

NAME \_\_\_\_\_

DISCIPLINE \_\_\_\_\_

NAME \_\_\_\_\_

AREA EVALUATED	CONDITION
Indications of Movement of Structural Items on Slopes	None observed
Trespassing on Slopes	None observed
Sloughing or Erosion of Slopes or Abutments	None observed
Rock Slope Protection - Riprap Failures	None
Unusual Movement or Cracking at or Near Toes	None
Unusual Embankment or Downstream Seepage	See narrative
Piping or Boils	None observed
Foundation Drainage Features	None
Toe Drains	None
Instrumentation System	None

PERIODIC INSPECTION CHECK LIST

PROJECT Harrisville Pond Dam DATE May 22, 1978

PROJECT FEATURE Outlet Works

DISCIPLINE Structures

PROJECT FEATURE \_\_\_\_\_

DISCIPLINE \_\_\_\_\_

DISCIPLINE \_\_\_\_\_

NAME John Doe

NAME \_\_\_\_\_

NAME \_\_\_\_\_

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - WASTE SLUICE OPENING</u>	
General Condition of Stonework	Fair
Erosion or Cavitation	None observed
Condition at Joints	Good
Gates	Two, manually operated
<u>OUTLET WORKS - PENSTOCK</u>	
Size	48-inch steel pipe
General Condition	Poor, has a hole near the dam
Gates	Two, manually operated

PERIODIC INSPECTION CHECK LIST

PROJECT Harrisville Pond Dam

DATE May 22, 1978

PROJECT FEATURE Spillway Weir

DISCIPLINE Structures

NAME John M. Miller

PROJECT FEATURE Approach Channel

DISCIPLINE Soils & Foundation

NAME Henry D. Miller

DISCIPLINE Hydraulics & Hydrology

NAME P. Eng. Michael J. Miller

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS</u>	
a. Approach Channel	
General Condition	Good
Loose Rock Overhanging Channel	None observed
Trees Overhanging Channel	None observed
Floor of Approach Channel	With water above crest elevation, floor not visible
b. Weir and Training Walls	
General Condition of Stonework	Good

PERIODIC INSPECTION CHECK LIST

PROJECT Harrisville Pond Dam DATE May 22, 1978

PROJECT FEATURE \_\_\_\_\_

DISCIPLINE \_\_\_\_\_

NAME \_\_\_\_\_

PROJECT FEATURE Discharge Channel

DISCIPLINE Soils & Foundation

NAME Henry H. Jell

DISCIPLINE Hydraulics & Hydrology

NAME L. W. MacIntire Jr.

AREA EVALUATED	CONDITION
<hr/>	
c. Discharge Channel	
General Condition	Good
Loose Rock	
Overhanging Channel	None observed
Trees Overhanging Channel	None observed
Floor of Channel	Good condition
Other Obstructions	None observed

PERIODIC INSPECTION CHECK LIST

PROJECT Harrisville Pond Dam DATE May 22, 1978

PROJECT FEATURE \_\_\_\_\_

DISCIPLINE \_\_\_\_\_ NAME \_\_\_\_\_

PROJECT FEATURE Rudimentary Type Weir  
Channels

DISCIPLINE Soils & Foundation

NAME Henry H. Miller

DISCIPLINE Hydraulics & Hydrology

NAME L. Paul Michael

AREA EVALUATED CONDITION

OUTLET WORKS - RUDIMENTARY TYPE WEIR,  
APPROACH AND DISCHARGE  
CHANNELS

a. Approach Channel

General Condition	Good
Loose Rock Overhanging Channel	None observed
Trees Overhanging Channel	None observed
Floor of Approach Channel	Could not be seen

b. Weir

General Condition	Fair condition, constructed with miscellaneous materials
-------------------	--

c. Discharge Channel

General Condition	Good
-------------------	------

PERIODIC INSPECTION CHECK LIST

PROJECT Harrisville Pond Dam DATE May 22, 1978

PROJECT FEATURE \_\_\_\_\_

DISCIPLINE \_\_\_\_\_

PROJECT FEATURE Rudimentary Type Weir  
Channels

NAME \_\_\_\_\_

DISCIPLINE Soils & Foundation

NAME Henry H. Miller

DISCIPLINE Hydraulics & Hydrology

NAME 1. P.C. McCormick

AREA EVALUATED	CONDITION
Loose Rock	
Overhanging Channel	None observed
Trees Overhanging Channel	None observed
Floor of Channel	Good condition
Other Obstructions	None observed

APPENDIX B

EXISTING AVAILABLE INFORMATION

✓ 0

## APPENDIX B

### 1. Listing of Records and their Location

New Hampshire Water Resources Board in Concord, New Hampshire, 37 Pleasant Street, have a file of records and correspondence from 1937-1977, filed under Town/Dam No. 109.08.

The documents of importance to design and maintenance are the following:

- (1) December 12, 1938. Two pages of data on Reservoirs and Water Developments in New Hampshire. By the New Hampshire Water Control Commission. Tabulated by AAN & RLT.
- (2) July 13, 1942. Questionnaire. Water Powers of New Hampshire. By the New Hampshire Water Resources Board. Signed by Mr. Joe L. Colony, Jr. (for the owner).
- (3) January 28, 1948. Questionnaire (similar to above).
- (4) March 18, 1977. Letter from Filtrine Manufacturing Co., Mr. John P. Hansel, president, to Mr. Vern Knowlton, New Hampshire Water Resources Board, regarding application for the right to operate the dams on Nubanusit Brook.

### 2. Copies of Past Inspection Records

Included with this report are the following past inspection reports:

- (1) October 8, 1937 - By the New Hampshire Water Resources Board, including sketches, some dimensions, two pages.
- (2) December 12, 1938 - By the New Hampshire Water Control Commission, tabulated by AAN & RLT, one page.
- (3) October 18, 1974 - By the New Hampshire Water Resources Board, one page.
- (4) December 12, 1975 - By the New Hampshire Water Resources Board, signed by Mr. S. Burritt. Includes a key plan with dimensions of openings, four pages.

NEW HAMPSHIRE WATER RESOURCES BOARD

INVENTORY OF DAMS AND WATER POWER DEVELOPMENTS

DAM

BASIN Herrimack NO. 8 109.08 "   
 RIVER PAULINGVILLE Branch MILES FROM MOUTH 1.5 D.A.S.Q.MI 17-050   
 TOWN PAULINGVILLE OWNER Checkers Mill   
 LOCAL NAME OF DAM Grindry Upperend   
 BUILT 1861 DESCRIPTION Brick 100' x 10' x 10'

POND AREA-ACRES 119.25 DRAWDOWN FT. 10-21 POND CAPACITY-ACRE FT. 1100000   
 HEIGHT-TOP TO BED OF STREAM-FT. 10-21 MAX. 10-21 MIN.   
 OVERALL LENGTH OF DAM-FT. 75 MAX. FLOOD HEIGHT ABOVE CREST-FT. 10-21   
 PERMANENT CREST ELEV.U.S.G.S. 720.05 LOCAL GAGE 720.05   
 TAILWATER ELEV.U.S.G.S. 720.05 LOCAL GAGE 720.05   
 SPILLWAY LENGTHS-FT. " 50 None FREEBOARD-FT. 10-21   
 FLASHBOARDS-TYPE, HEIGHT ABOVE CREST " "   
 WASTE GATES-No. 1 6 MAX. OPENING DEPTH SILL BELOW CREST 15 below top   
1 6 6 15 below top penstock gate

REMARKS Condition fair. Condition under old building such as to undermine foundation if gate wide open.

30' into stream, 1-1/2' above stream bed, 10' above top of dam.

POWER DEVELOPMENT

Coordinates 42° 55' + 0500 yds,  
72° 05' + 1250 yds.

UNITS NO.	RATED HP	HEAD FEET	C.F.S. FULL GATE	KW	MAKE
	475	10	"		
	tot. 81300000	30000000	USGS list		

USE Water power for wooden mill.

REMARKS Primary H.P. 4.9, i.e. June 27.3

A.E. act. in connection with dam from F. S. Sandstrom C-220  
Should Chief Engineer Old mill now is planted up as per sketch.  
4' dia steel penstock to upper mill 260' Power taken to stone mill  
by out door rope drive. Waste gate under old building, water goes to  
pond above stone mill. New brick building electrically operated by bought  
current.

10/27/36 AE

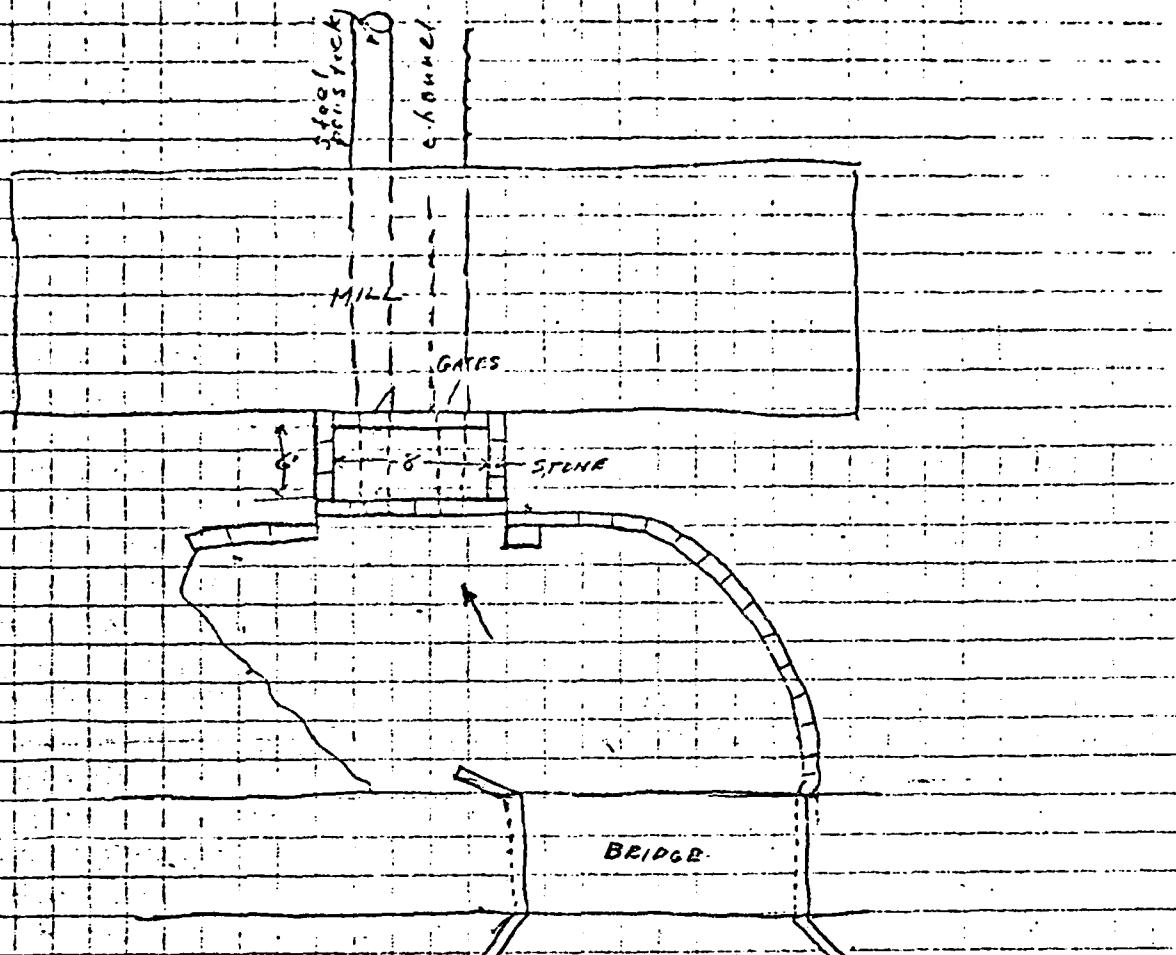
B-2

DATE 1975

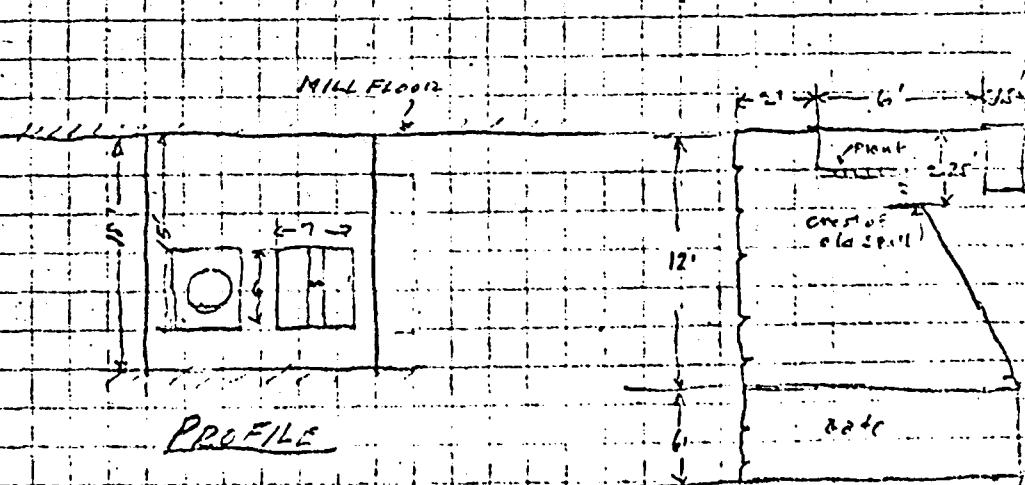
10/27/36

HARRISVILLE POND DAM-HARRISVILLE

109.08



PLAN



## PROFILE

!B-3

Penstock faces  
and waste gate  
open under  
building

## DATA ON DAMS IN NEW HAMPSHIRE

## LOCATION

STATE NO. 103.08

Town ..... Harrisville ..... County ..... Cheshire .....  
 Stream ..... Harrisville Pond .....  
 Basin-Primary ..... Merrimack R. ..... Secondary ..... Nubanusit Brook .....  
 Local Name .....  
 Coordinates—Lat. ..... 42° 55' + 10,500' ..... Long. ..... 72° 05' + 3750' ..... *8.64 D.P.T.*

## GENERAL DATA

Drainage area: Controlled ..... Sq. Mi.: Uncontrolled ..... Sq. Mi.: Total 11 ..... Sq. Mi.  
 Overall length of dam ..... 75' ft.: Date of Construction ..... 1885 .....  
 Height: Stream bed to highest elev. ..... 21' ft.: Max. Structure ..... ft.  
 Cost—Dam ..... : Reservoir .....  
*8.64 D.P.T.*

## DESCRIPTION Masonry- Stone Earth &amp; Concrete

## Waste Gates

Type .....  
 Number ..... 1 ..... Size ..... 6 ..... ft. high x ..... 6 ..... ft. wide  
 Elevation Invert ..... 15 ..... : Total Area ..... 36 ..... 72 ..... sq. ft.  
 Hoist .....  
*8.64 D.P.T.*

## Waste Gates Conduit

Number ..... : Materials .....  
 Size ..... ft.: Length ..... ft.: Area ..... sq. ft.

## Embankment

Type .....  
 Height—Max. ..... ft.: Min. ..... ft.  
 Top—Width ..... : Elev. ..... ft.  
 Slopes—Upstream ..... on ..... : Downstream ..... on .....  
 Length—Right of Spillway ..... : Left of Spillway .....  
*8.64 D.P.T.*

## Spillway

Materials of Construction ..... (none) .....  
 Length—Total ..... ft.: Net ..... ft.  
 Height of permanent section—Max. ..... ft.: Min. ..... ft.  
 Flashboards—Type ..... : Height ..... ft.  
 Elevation—Permanent Crest ..... : Top of Flashboard .....  
 Flood Capacity ..... cfs.: ..... cfs/sq. mi.

## Abutments

Materials: .....  
 Freeboard: Max. ..... ft.: Min. ..... ft.

Headworks to Power Devel.—(See "Data on Power Development")

OWNER ..... Cheshire Mills .....  
 Power - Woolen Mill ..... *8.64 D.P.T.*

## REMARKS

B-4

Tabulation By ..... A. A. N. & R. L. T. ..... Date ..... December 12, 1933.

DAM SAFETY INSPECTION REPORT FORMTown: Harrisville Dam Number: 109.03Inspected by: ESB Date: 10 Oct 1974

Local name of dam or water body: \_\_\_\_\_

Owner: \_\_\_\_\_ Address: \_\_\_\_\_

Owner was/was not interviewed during inspection.

Drainage Area: \_\_\_\_\_ sq. mi. Stream: \_\_\_\_\_

Pond Area: \_\_\_\_\_ Acre, Storage \_\_\_\_\_ Ac-Ft. Max. Head \_\_\_\_\_ Ft.

Foundation: Type \_\_\_\_\_, Seepage present at toe - Yes/No, \_\_\_\_\_

Spillway: Type 51cpl, Freeboard over perm. crest: 2.5Width 3.5' x 2.5', Flashboard height None

Max. Capacity \_\_\_\_\_ c.f.s.

Embankment: Type \_\_\_\_\_, Cover \_\_\_\_\_ Width \_\_\_\_\_

Upstream slope \_\_\_\_\_ to 1; Downstream slope \_\_\_\_\_ to 1

Abutments: Type \_\_\_\_\_, Condition: Good, Fair, Poor \_\_\_\_\_

Gates or Pond Drain: Size 2x3 ft Capacity \_\_\_\_\_ Type Rock PinchLifting apparatus \_\_\_\_\_ Operational condition ?

Changes since construction or last inspection:

Downstream development: \_\_\_\_\_

This dam would not be a menace if it failed.

Suggested reinspection date: \_\_\_\_\_

Remarks: Some leaks 4' Finstock A/T road

NEW HAMPSHIRE  
WATER RESOURCES BOARD

SITE EVALUATION DATA

OWNER: John Colby Jr TELEPHONE NO. \_\_\_\_\_

MAILING ADDRESS: Harrisville

SITE LOCATION (TOWN OR CITY) Harrisville

NAME OF STREAM OR WATERBODY: Harrisville

QUADRANGLE: \_\_\_\_\_ LOCATION \_\_\_\_\_

HEIGHT OF (PROPOSED, EXISTING) DAM 21 LENGTH 75'

TYPE OF (PROPOSED, EXISTING) STRUCTURE \_\_\_\_\_

DRAINAGE AREA 10.95 m POND AREA 119 A

AVAILABLE ARTIFICIAL STORAGE: PERMANENT: \_\_\_\_\_ TEMPORARY: \_\_\_\_\_ TOTAL 2.002

EXISTING DEVELOPMENT DOWNSTREAM OF (PROPOSED, EXISTING) STRUCTURE Shop

Mill other dams

POTENTIAL DEVELOPMENT DOWNSTREAM OF (PROPOSED, EXISTING) STRUCTURE Limited

POTENTIAL DAMAGE DOWNSTREAM OF STRUCTURE (EXPLAIN IN DETAIL AND INCLUDE ANY POTENTIAL LOSS OF LIFE ESTIMATE)

Wash out of Toy shop and  
damage to mill Possible loss of life  
from people in mill

OTHER COMMENTS: \_\_\_\_\_

CLASS OF STRUCTURE -- NON MENACE MENACE C DAM # 109.08

DATE OF INSPECTION: 12 Dec 75

SIGNED

8th CB, Jr

SIGNATURE

DATE:

## NEW HAMPSHIRE WATER RESOURCES BOARD

INSPECTION REPORTTown: Harrisville Dam Number: 109.03Name of Dam, Stream and/or Water Body: Harrisville LakeOwner: Tony Cilony Jr. Telephone Number: \_\_\_\_\_Mailing Address: HarrisvilleMax. Height of Dam: 21' Pond Area: 119.34 Length of Dam: 75'FOUNDATION: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_OUTLET WORKS: Spillway 3' 7" wide 2.5' FreeboardOverflow 2" higher than Spillway goes under  
Road with 4' Dia Culvert. Water from overflow  
comes in below mill4 gates 2'x3' all work 2 go to penstock  
PenstockABUTMENTS: Granite face with earth. Behind Good Shape  
\_\_\_\_\_EMBANKMENT: \_\_\_\_\_  
\_\_\_\_\_

SPILLWAY: Length: 3' 7" Freeboard: 2' 6"

SEEPAGE: Location, estimated quantity, etc.

San Joaquin Through Left side ground settled  
on embankment above outlet

Changes Since Construction or Last Inspection:

\_\_\_\_\_

Tail Water Conditions:

Tail water has Annex 3x3 outlet through bld.

Overall Condition of Dam: Fair

Contact With Owner: Yes

Date of Inspection: 12 Dec 75 Suggested Reinspection Date 1977

Class of Dam: Menace C

Signature J. Burnell

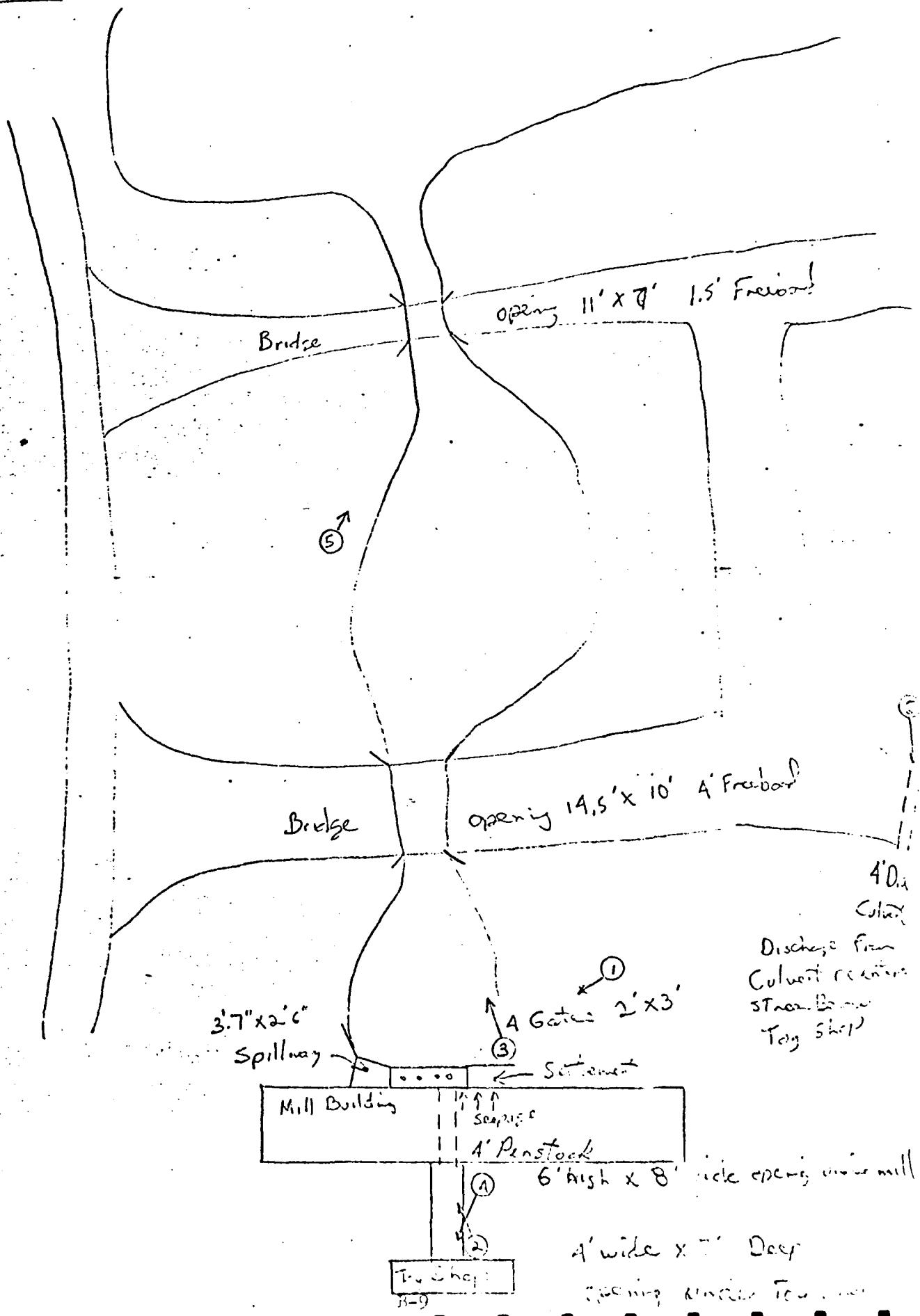
Date \_\_\_\_\_

-3-

Dam No. 109,23

COMMENTS:

Reacts below overflow crest at culvert should  
be removed to improve flow



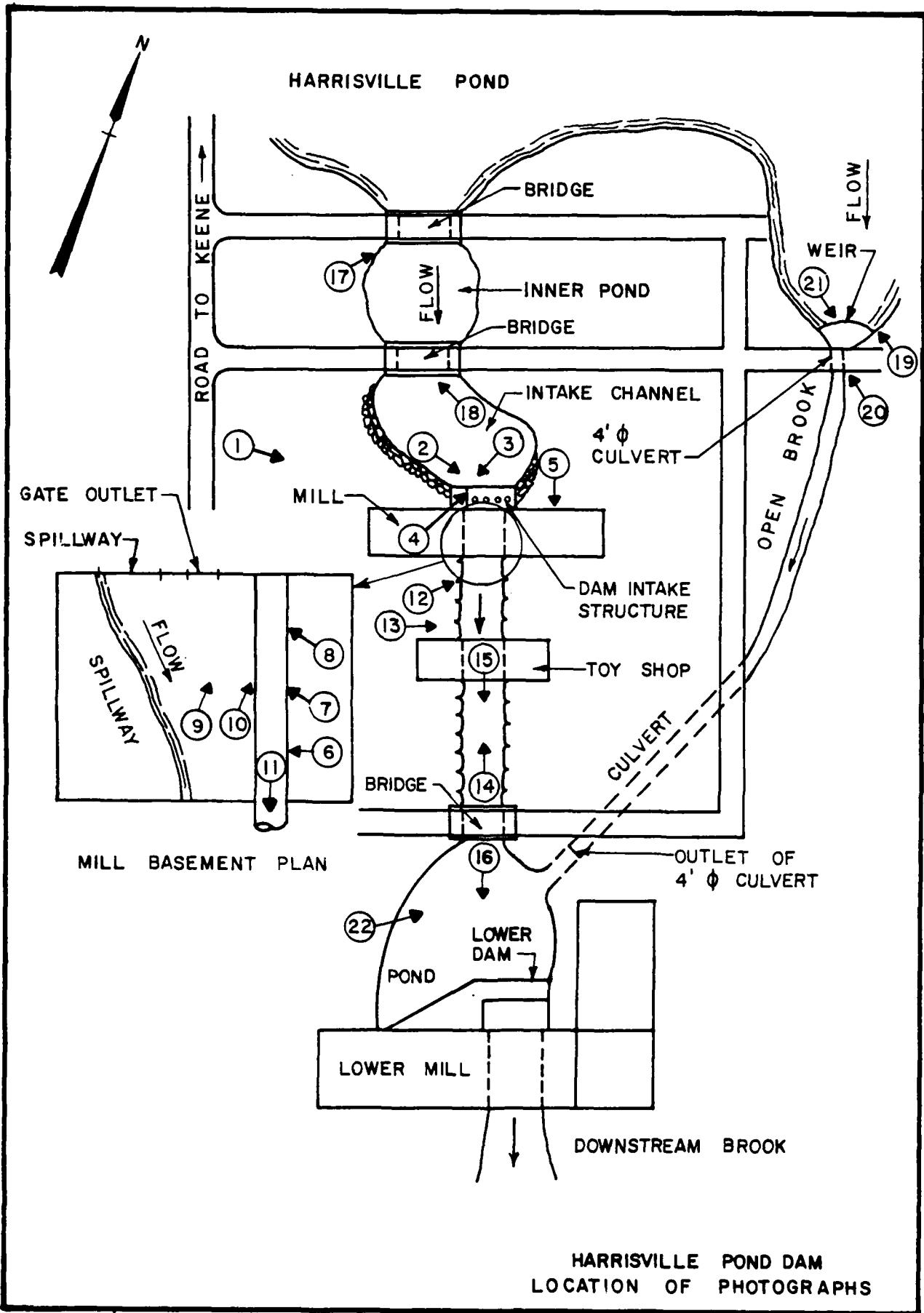
APPENDIX C  
PHOTOGRAPHS

APPENDIX C

REPRESENTATIVE PHOTOGRAPHS OF PROJECT

		<u>Page</u>
<u>LOCATION PLAN</u>		
Plan 1 - Location of Photographs Taken May 22, 1978		C-3
<u>PHOTOGRAPHS</u>		
<u>No.</u>	<u>Negative No.</u>	<u>Page</u>
1. Intake Channel and the Dam Intake Structure, Looking Northeast.	1-17	C-4
2. Intake Structure, Right - Intake Conduit to Spillway Mill Building Built on Top of Dam.	1-13	C-4
3. Rack-and-Pinion Gate Operators Over the Intake Structure.	1-16	C-5
4. Detail of Rack-and-Pinion Gate Operators.	1-20	C-5
5. Settlement of Backfill Near the Intake Structure, Looking Downstream into the Basement Window.	3-18A	C-6
6. Columns Supporting the Mill Floor Over the Basement Which is Part of the Downstream Channel.	3-12A	C-6
7. Dam Looking Upstream from the Basement of the Mill; Left - Spillway; Right - Abandoned Penstock; Center - Sluice Opening.	1-12	C-7
8. Spillway and Sluice Opening, Looking Upstream, Inside of the Basement.	3-15A	C-7
9. Penstock, Upper End, With a Hole On Top Near the Intake Structure.	3-14A	C-8

<u>No.</u>	<u>Negative No.</u>	<u>Page</u>
10. Dam Masonry Looking Upstream from the Basement of the Mill, Abandoned Penstock to the Left.	3-17A	C-8
11. Penstock (Abandoned), Lower End and the Downstream Channel, Looking from the Basement of Mill Building.	3-13A	C-9
12. Penstock Coming Out of the Basement of Mill Building.	2-8	C-9
13. Upper Mill (Over the Dam) and the Toy Shop (Right), Downstream Channel Below these Buildings.	1-18	C-10
14. Downstream Channel Looking Up, Toy Shop Straddles this Channel, the Upper Mill is in Background, with the Dam Under it.	1-9	C-10
15. Downstream Channel, Looking from the Toy Shop.	2-6	C-11
16. Lower Mill and Pond, Looking from the Road below the Toy Shop.	2-11	C-11
17. Bridge Over Channel from Harrisville Pond to the Inner Pond.	3-20A	C-12
18. Bridge Over Intake Channel from the Inner Pond to the Dam, Looking Upstream.	3-22A	C-12
19. Harrisville Pond Looking West, with Overflow Weir in Front.	1-4	C-13
20. Four-Foot Diameter Culvert Looking West, Upstream.	1-3	C-13
21. Four-Foot Diameter Culvert Looking East, Downstream.	1-2	C-14
22. Discharge of Four-Foot Diameter Culvert to the Pond Below the Toy Shop.	1-11	C-14





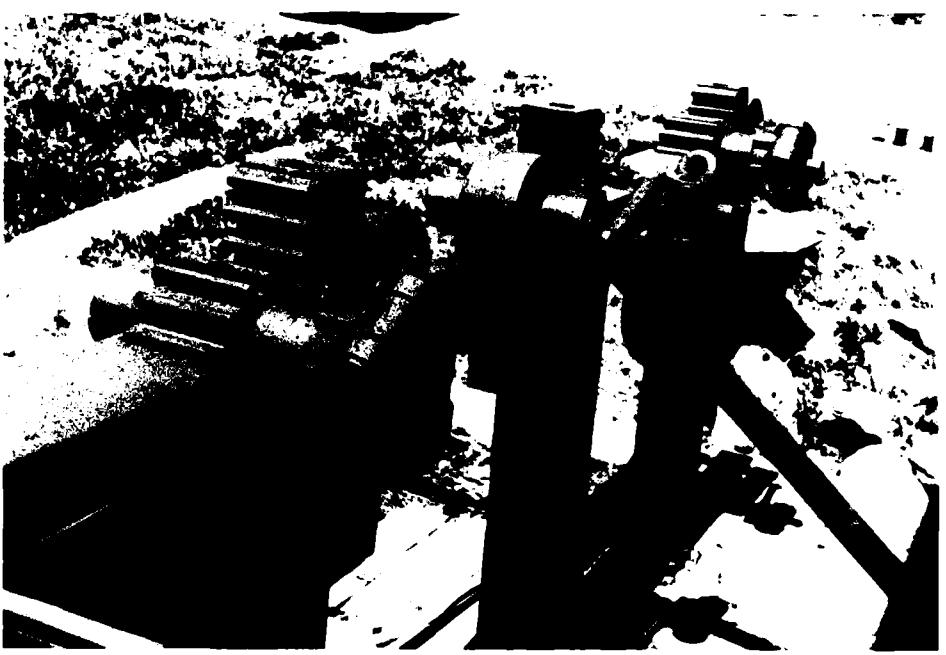
1. Intake Channel and the Dam Intake Structure,  
Looking Northeast.



2. Intake Structure. Right - Intake Conduit to Pelton.  
Mill Building Built on Top of Dam.



3. Rack-and-Pinion Gate Operators Over the Intake Structure.



4. Detail of Rack-and-Pinion Gate Operators.

5. Settlement of Backfill Near the Intake Structure, Looking Downstream into the Basement Window



6. Columns Supporting the Mill Floor Over the Basement Which is Part of the Downstream Channel.



7. Dam Looking Upstream from the Basement of the Mill...  
Left - Spillway; Right - Abandoned Penstock;  
Center - Sluice Opening.



8. Spillway and Sluice Opening - Mill Building  
Inside of the Basement.



9. Penstock, Upper End, With a Hole on Top Near the Intake Structure.



10. Dam Masonry Looking Upstream from the Basement of the Mill. Abandoned Penstock to the Left.



11. Penstock (Abandoned), Lower End and the Downstream Channel, Looking from the Basement of the Mill Building.



12. Penstock Coming Out of the Basement of Mill Building.



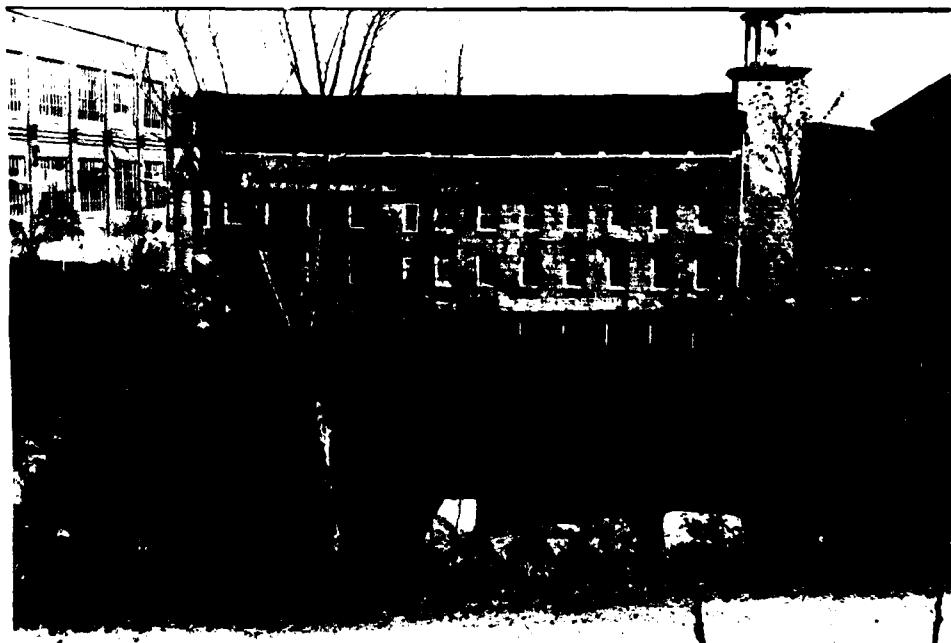
13. Upper Mill (Over the Dam) and the Toy Shop (Right).  
Downstream Channel Below These Buildings.



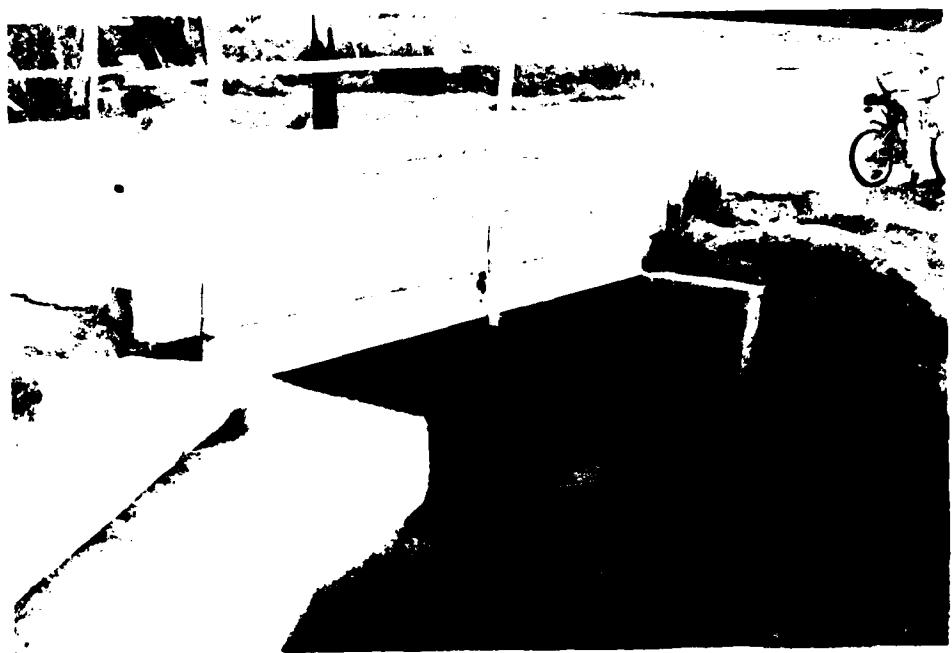
14. Downstream Channel Looking Up. Toy Shop Straddles  
this Channel, the Upper Mill is in Background With  
the Dam Under it.



15. Downstream Channel, Looking from the Toy Shop.



16. Lower Mill and Pond, Looking from the Road Below the Toy Shop.



17. Bridge over channel from Harrington Point to  
Inner Point.



18. Bridge over inlet the channel from the outer point to  
Inner Point, in King's Harbor.



19. Harrisville Pond Looking West, With overexposed Water in Front.



19. Four-Foot Diameter Culvert Looking West, Overexposed.



21. Four-Foot Diameter Culvert Looking East, Downstream.



22. Discharge of Four-Foot Diameter Culvert to the River Below the Toy Shop.

APPENDIX D

HYDROLOGIC & HYDRAULIC COMPUTATIONS

SUBJECT APTUWILL DAM INSP. PROGRAM  
HARRISVILLE POND DAM.

TOTAL Storage area of Harrisville Pond  
at 3 am

$$= 16.6 \text{ square miles}$$

The drainage area of Harrisville Pond is  
characterized by rolling topography. Hence,  
from guide curves furnished by the Corps  
of Engineers, it is found that

Probable maximum flood Peak inflow

$$= 1650 \times 10 \text{ cfs}$$
$$= 16,500 \text{ cfs.}$$

According to size classification, Harrisville  
Pond dam is intermediate in size.

According to hazard classification, Harrisville  
dam falls under the category of high hazard dam.

Therefore, the adopted spillway test flood  
Peak inflow ( $Q_p$ ) = 16,500 cfs

SUBJECT HARVEYVILLE POND

SPILLWAY TEST FLOOD INFLOW HYDROGRAPH

Max. Length of travel = 31,700 ft.

Diff. in Elevation = 466 ft.

$$\begin{aligned} T_c &= \frac{(31,700)^{1.15}}{7700 \times (466)^{0.138}} \text{ hrs} \\ &= \frac{1500.44}{7700 \times 10.327} \\ &= 1.886 \text{ hrs.} \\ &\approx 2.0 \text{ hrs.} \end{aligned}$$

SPILLWAY TEST FLOOD PEAK INFLOW = 16,500 cfs.

SUBJECT ALERICVILLE P-110SPILLWAY TEST FLOOD INFLOW HYDROGRAPH  
(BASED ON SCS DIMENSIONLESS HYDROGRAPH)

$$T_c = 2.0 \text{ hrs}$$

$$Q_p = 16,500 \text{ hrs.}$$

<u>T (hrs)</u>	<u>T/Tc</u>	<u>Q/Qp</u>	<u>Q (cfs)</u>
0.50	0.25	0.05	825
1.00	0.50	0.18	2970
1.50	0.75	0.73	12045
2.00	1.00	1.00	16500
2.50	1.25	0.80	13200
3.00	1.50	0.40	6600
3.50	1.75	0.25	4125
4.00	2.00	0.17	2805
5.50	2.75	0.06	990
7.00	3.50	0.02	330
8.00	4.00	0.01	165

SUBJECT HARRISVILLE POND DAM  
ESTIMATION OF CAPACITY CURVEFILE NUMBER EN-001  
SHEET NUMBER 4/13  
DATE 7-26-1972  
COMPUTED BY DEM  
CHECKED BY \_\_\_\_\_

It is assumed that the溢流坝 crest ELEV.

= 1318.0

surface area of lake at ELE. 1318 = 114.0 acres

ELEVATION	STORAGE (acre-feet)
1318.0	2000
1318.5	2060
1319.0	2119
1320.0	2239
1321.0	2358
1322.0	2478
1325.0	2835
1330.0	3432
1335.0	4029

SUBJECT HARVEYVILLE PONDDISCHARGE RATING TABLE FOR THE  
WASTE SLUICE

INVERT ELEVATION OF WASTE SLUICE = 1305.3

ELEVATION OF THE CENTER OF SLUICE = 1308.3

HEAD OF WASTE SLUICE =  $4 \times 6 = 24$  ft. 0 in.

Assume

 $C_d = 0.45$  (from p. 537 for free discharge).

$$Q_{W.S.} = C_d \cdot A \cdot \sqrt{2gT} = 0.45 \times 24 \times 8 \sqrt{T}$$

$$= 86.4 \sqrt{T}$$

<u>ELEV.</u>	<u>Y</u>	<u><math>Q_{W.S.}</math></u>
1318	9.70	269.0
1318.5	10.20	276.0
1319.0	10.70	283.0
1319.5	11.20	289.0
1320.0	11.70	296.0
1320.5	12.20	302.0
1321.5	13.20	314.0
1322.5	14.20	326.0
1323.5	15.20	337.0
1324.5	16.20	348.0
1325.5	17.20	358.0
1326.5	18.20	369.0
1328.5	20.20	388.0
1330.5	22.20	407.0
1332.5	24.20	425.0
1329.4	21.10	397.0

SUBJECT HERRISVILLE POND DAM

DISCHARGE RATING TABLE FOR  
SPILLWAY.

Assume that the Spillway crest ELEV = 1318.0

SPILLWAY LENGTH = 3 feet 7 inches  
= 3.58 feet.

The height of opening in the wall above the  
spillway crest = 2.5 feet.

It is assumed here that the elevation of the  
Country road above 4 feet diameter road culvert  
piles = 1320.5.

It means, that as soon as the water surface  
elevation in the pond rises to ELEV. 1320.5 during  
floods, there will be overflow over the roadway.  
It is also assumed that the effective length of the  
roadway = 200 feet.

DISCHARGE OVER SPILLWAY.

HEAD ELE.

$H_1 = 0.5$	1318.5	$Q_s = 2.8 \times 3.58 \times (0.5)^{3/2} = 3.5 \text{ cfs}$
$H_1 = 1.0$	1319.0	$Q_s = 2.8 \times 3.58 \times 1 = 10.0 \text{ cfs}$
$H_1 = 1.5$	1319.5	$Q_s = 2.8 \times 3.58 \times (1.5)^{3/2} = 18.4 \text{ cfs}$
$H_1 = 2.0$	1320.0	$Q_s = 2.8 \times 3.58 \times (2)^{3/2} = 28.35 \text{ cfs}$
$H_1 = 2.5$	1320.5	$Q_s = 2.8 \times 3.58 \times (2.5)^{3/2} = 39.59 \text{ "}$

For  $H_1 > 2.5$ , the opening functions as a rectangular  
orifice.

$$Q = C \cdot A \cdot \sqrt{2gh}$$

Let  $C = 0.54$ .

SUBJECT HARPSICHELL POND DAM  
DISCHARGE RATING TABLE FOR  
SPILLWAY.

$$A = 3.58 \times 2.5 = 8.95 \text{ ft}^2$$

$$C A \sqrt{2g} = 0.54 \times 8.95 \times 8.02 = 38.76$$

$$Q = 38.76 \sqrt{h}$$

$$H_1 = 3.5 \quad 1321.5 \quad Q_s = 38.76 \sqrt{2.25} = 58.0 \text{ cfs}$$

$$H_1 = 4.5 \quad 1322.5 \quad Q_s = 38.76 \sqrt{3.25} = 70.0 \text{ "}$$

$$H_1 = 5.5 \quad 1323.5 \quad Q_s = 38.76 \sqrt{4.25} = 80.0$$

$$H_1 = 6.6 \quad 1324.5 \quad Q_s = 38.76 \sqrt{5.25} = 89.0$$

$$H_1 = 7.5 \quad 1325.5 \quad Q_s = 38.76 \sqrt{6.25} = 97.0$$

$$H_1 = 8.5 \quad 1326.5 \quad Q_s = 38.76 \sqrt{7.25} = 104.0$$

$$H_1 = 10.5 \quad 1328.5 \quad Q_s = 38.76 \sqrt{9.25} = 118.0$$

$$H_1 = 12.5 \quad 1330.5 \quad Q_s = 38.76 \sqrt{11.25} = 130.0$$

$$H_1 = 14.5 \quad 1332.5 \quad Q_s = 38.76 \sqrt{13.25} = 141.0 \text{ "}$$

$$@ H_1 = 11.40 \quad Q_s = 38.76 \sqrt{10.15} = 123.0 \text{ "}$$

SUBJECT HARRISVILLE POND DAMGATING TABLE FOR ROADWAY

$$Q = 2.6 \times 200 \times H^{3/2}$$

$$= 520 H^{3/2}$$

<u>H</u>	<u>ELEVATION</u>	<u><math>Q_2 = 520H^{3/2}</math></u>
1.0	1321.5	520.0
2.0	1322.5	1471.0
3.0	1323.5	2702.0
4.0	1324.5	4160.0
5.0	1325.5	5814.0
6.0	1326.5	7642.0
8.0	1328.5	11766.0
10.0	1330.5	16444.0
12.0	1332.5	21,615.0

Discharge through the 4 foot diameter pipe culvert under the roadway is ignored as its contribution is negligibly small. It is also assumed that the invert elevation of the pipe culvert is about 7-feet below the top of roadway. That is, invert elevation of pipe culvert = 1313.5.

SUBJECT HARRISVILLE POND DAMCOMPOSITE DISCHARGE RATING

## TABLE.

ELEV.	SPILLWAY	WASTE	FLOWOVER	TOTAL
	DISCHARGE	SUICE	ROADWAY	$Q$
	$Q_s$	$Q_{W.S}$	$Q_{R.W.}$	
1318.0	0.0	269		269.0
1318.5	3.5	276		280.0
1319.0	10.0	283		293.0
1319.5	18.4	289		308.0
1320.0	28.35	296		324.0
1320.5	39.59	302	0.0	342.0
1321.0	58.00	314	521.0	893.0
1322.5	70.00	326	1471.0	1867.0
1323.5	80.00	337	2702.0	3119.0
1324.5	89.00	348	4160.0	4597.0
1325.5	97.00	358	5814.0	6269.0
1326.5	104.00	369	7642.0	8115.0
1328.5	118.00	388	11766.0	12272.0
1330.5	130.00	407	16444.0	16981.0
1332.5	141.00	425	21615.0	22181.0

DISCHARGE THROUGH PIPE CULVERT @ ELEV. 1239.40

Assume Type 5 flow i.e. the culvert entrance is submerged, and the tailwater is below the crest at the outlet.

$$Q = C A_D \sqrt{2g(h_1 - z)}$$

$$\frac{h_1 - z}{D} = \frac{15.9}{4} = 4.0$$

$$C = 0.72$$

$$Q = 0.72 \times \frac{\pi}{4} \times 4^2 \cdot \sqrt{64.4 \times 15.9} \quad (\text{Assume } z = 0)$$

$$= 9.068 \times 32.0$$

$$= 290.0 \text{ cfs.}$$

SUBJECT HARRISVILLE POND DAM  
TO DETERMINE PEAK CUTFLOW

SPILLWAY TEST FLOOD PEAK INFLOW ( $Q_p$ )  
= 16,500 cfs

TRIAL #1:

Assume inflow volume = 19" of runoff from D.A.

Available surcharge storage up to top of  
roadway above emergency spillway outlet  
Pipeline 7 feet above spillway crest.

$$= \frac{119 \times 7.0}{10 \times 640} \times 12$$

= 1.56 inches of runoff from D.A.

$$\frac{\text{Pond Surcharge Storage}}{\text{Inflow Runoff Vol.}} = \frac{1.56}{19} \\ = 0.082$$

Referring to Figure 17-11 in SCS NEH, Section 4

$$\frac{\text{Outflow Peak Rate}}{\text{Inflow Peak Rate}} = 0.94$$

$$\therefore \text{Outflow Peak Rate} = 0.94 \times 16500 \\ = 15,510 \text{ cfs.}$$

SUBJECT - ARRISVILLE POND DAM  
TO DETERMINE PEAK CUTOFF

TRIAL #2 :

From the composite rating curve, the above  
cutoff peak rate corresponds to  
ELEV. 1329.90

i.e. surcharge height above the spillway crest  
= 11.90 feet.

∴ Vol. of surcharge storage (STOR<sub>1</sub>)

$$= \frac{119 \times 11.90}{10 \times 640} \times 12$$

= 2.655 inches of runoff from D.A.

$$\begin{aligned} \therefore \text{Peak outflow } Q_{P_2} &= Q_p \left(1 - \frac{STOR_1}{19}\right) \\ &= 16,500 \left(1 - \frac{2.655}{19}\right) \\ &= 16500 \left(1 - 0.140\right) \\ &= 14,190 \text{ cfs.} \end{aligned}$$

SUBJECT HIRRISVILLE FOND DAM  
TO DETERMINE PEAK CUTFLOW:

TRIAL #3:

From the composite discharge rating curve  
the above outflow peak rate corresponds to  
ELEV. 1329.35

i.e. Surcharge ht. above the spillway crest  
= 11.35 feet.

∴ Vol. of Surcharge storage (stor.)

$$= \frac{119 \times 11.35}{10 \times 640} \times 12$$

= 0.211 inches of runoff from D.A.

∴ Peak outflow  $Q_{P_2} = 16,500 \left(1 - \frac{0.211}{19}\right)$

$$= 16,500 \left(1 - 0.011\right)$$

$$= 14,685 \text{ cfs.}$$

SUBJECT HIPPSVILLE POND DAM  
TO DETERMINE PEAK OUTFLOW

TRIAL # 4:

From the composite discharge rating curve  
the above outflow Peak Rate corresponds to  
ELEV. 1329.5

i.e. Surcharge ht. above the spillway crest  
= 11.5 feet.

i. Vol. of Surcharge storage (S42R1)

$$= \frac{119 \times 11.5}{10 \times 640} \times 12$$

= 2.566 inches of runoff from D.A.

i. Peak outflow  $Q_{P_2} = 16,500 \left(1 - \frac{2.566}{19}\right)$

$$= 16,500 \left(1 - 0.135\right)$$

$$= \underline{\underline{14,272.0 \text{ cfs.}}}$$

SUBJECT HARRIESVILLE POND D.A.  
TO DETERMINE PEAK OUTFLOW

TRIAL # 5 :

From the composite discharge rating curve, the  
above outflow peak rate corresponds to  
ELEV. 1329.35

i.e. sucharge ht. above the Spillway crest  
= 11.35 feet

Vol. of sucharge storage (STOR<sub>1</sub>)

$$= \frac{119 \times 11.35}{10 \times 640} \times 12$$

= 2.53 inches of runoff from D.A.

Average of STOR<sub>1</sub> and STOR<sub>2</sub>

$$= \frac{2.561 + 2.53}{2}$$

= 2.548 inches of runoff from D.A.

$$\therefore \text{PEAK OUTFLOW} = 16,500 \left(1 - \frac{2.548}{19}\right)$$

$$= 16,500 (1 - 0.134)$$

$$= 14,289 \text{ cfs.}$$

SUBJECT HARVESSVILLE POND DAM  
TO DETERMINE PEAK OUTFLOW.

FILE NUMBER EN-006

SHEET NUMBER 15 OF

DATE 11-6-1928

COMPUTED BY VPM

CHECKED BY

∴ The corresponding maximum port  
elevation = 1329.40

∴ Maximum surcharge ht = 11.40 feet.

At the maximum port elevation, the spillway can  
pass 123.0 cfs.

Here, the question of overtopping the dam does  
not arise as the dam forms the foundation of  
the northern wall of a two-story mill building.

Roadway over the culvert pipe would be  
overtopped by 8.9 feet.

Without overtopping the roadway, (i.e. at ELEV.  
1320.5), the spillway and the waste sluice  
together can pass only about 342 cfs.

That is about 2.5% of the test flood  
PEAK OUTFLOW.

SUBJECT HARRISVILLE POND DAM

ESTIMATION OF DEPTH OF FLOOD

WATER IN THE VICINITY OF DAMAGE  
IMPACT AREA DUE TO BREACH IN THE  
DAM AT RESERVOIR FULL CONDITION.

As explained in section 1.2d, it is not possible to generate downstream dam failure hydrograph in the vicinity of damage impact area, using a USGS topo map on which the contours are at 20-foot intervals.

Besides, no other topographic map is available for the area.

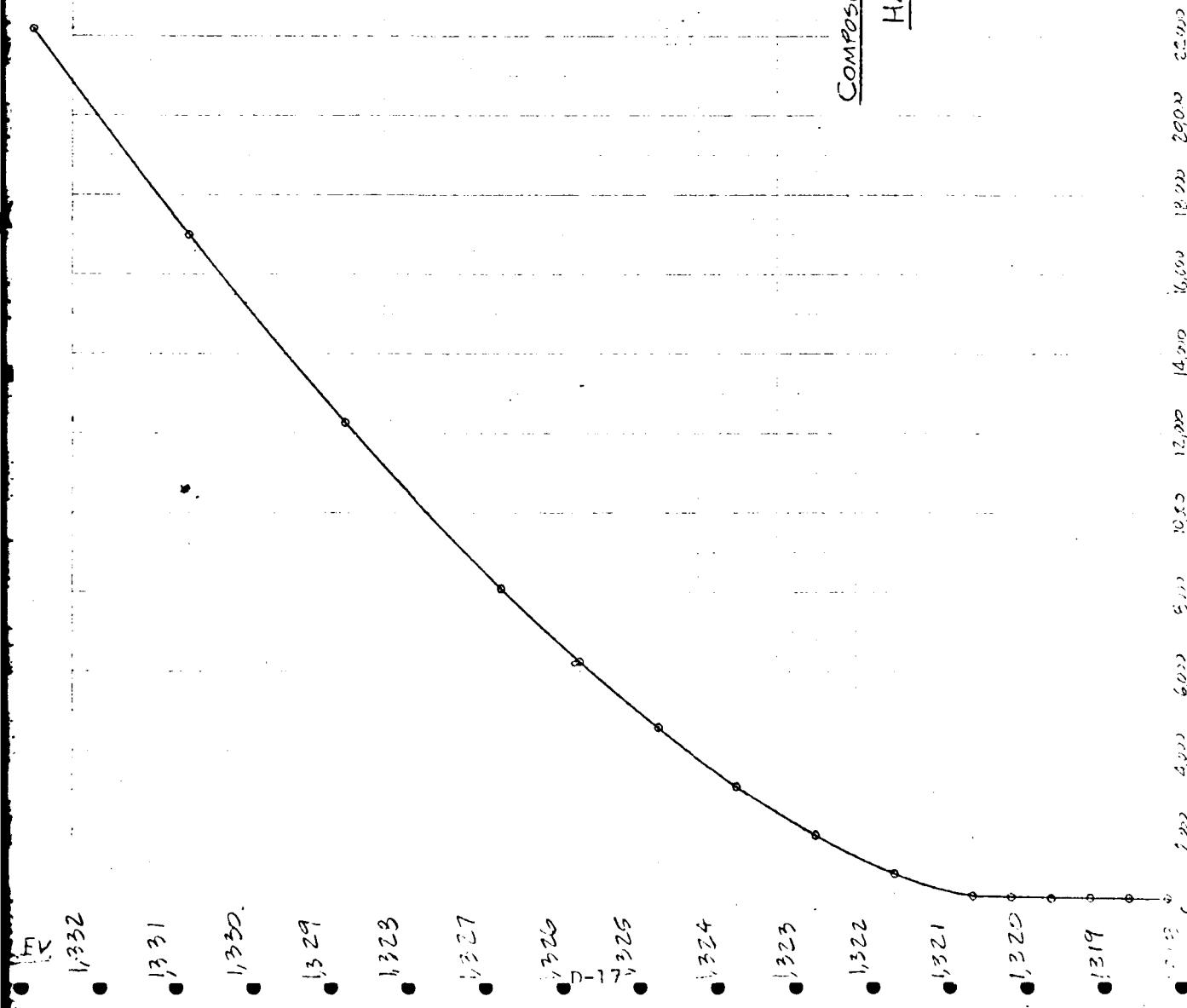
From the knowledge of the damage impact area, in the vicinity of Eastview village which is at a distance of  $2\frac{1}{2}$  miles downstream of Harrisville pond dam, a half park estimate has been made as follows:

Depth of water above the dam failed at F.R.L

$$\begin{aligned} &= 1318 - 1297 \\ &= 21 \text{ feet.} \end{aligned}$$

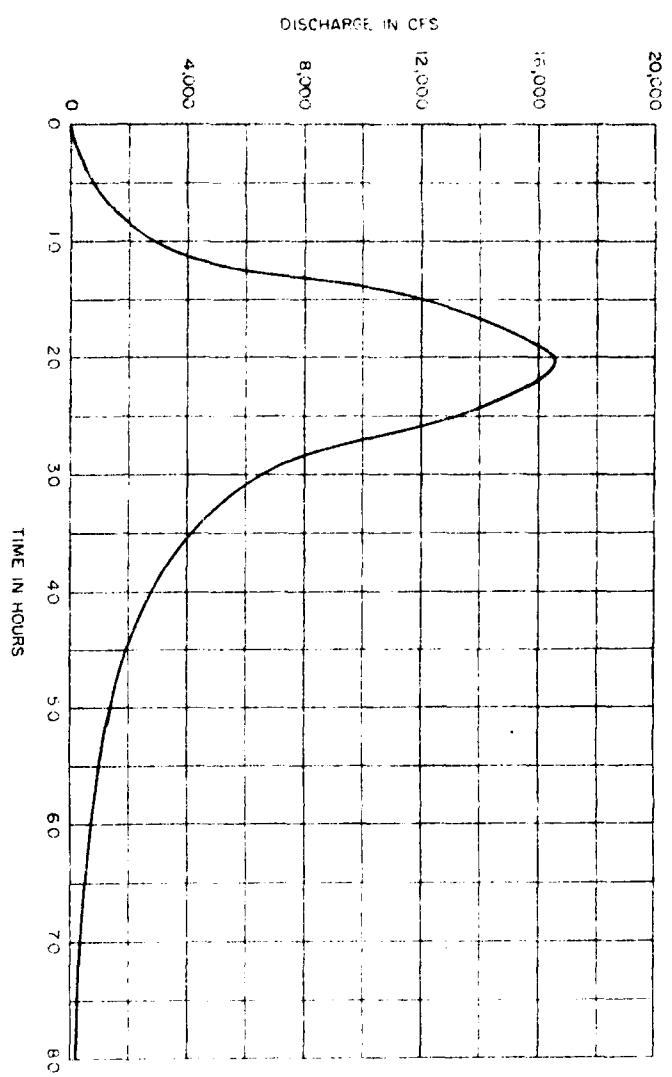
Height of flood wave at damage impact area is estimated to be about 14 feet.

Width of water spread at damage impact area is approximately indicated on the USGS map included in APPENDIX - D.



COMPOSITE DISCHARGE RATING CURVE

HARRISVILLE PONTO DAM

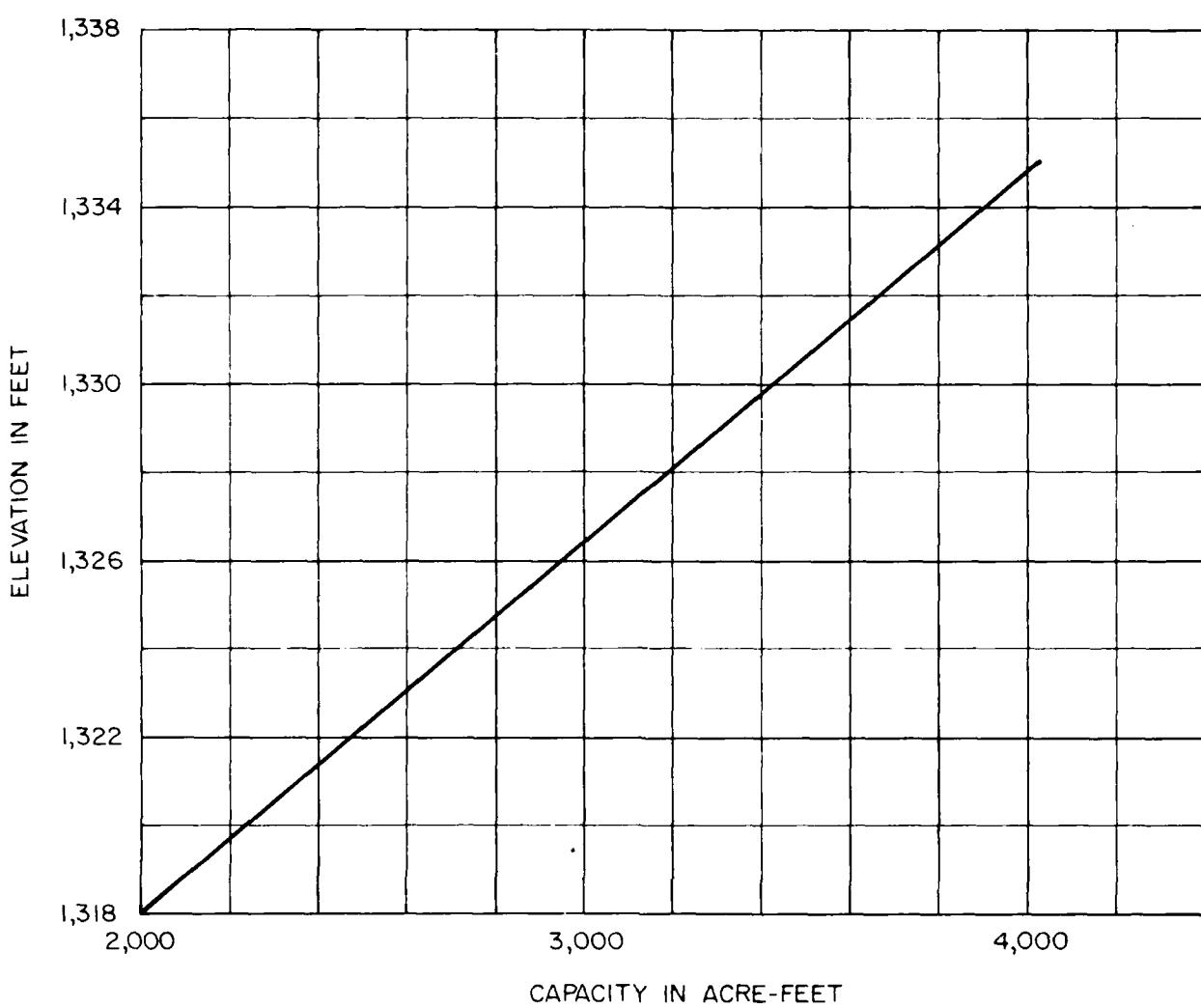


SPILLWAY TEST FLOOD INFLOW HYDROGRAPH

EN. PROFESSOR RICHARD J. MC AULIFFE, NEW ENGLAND  
ENGINEERING CO., INC., NEW HAMPSHIRE  
BOSTON, MASS.  
NATIONAL PROGRAM OF INSPECTION OF NON-FEDERAL DAMS

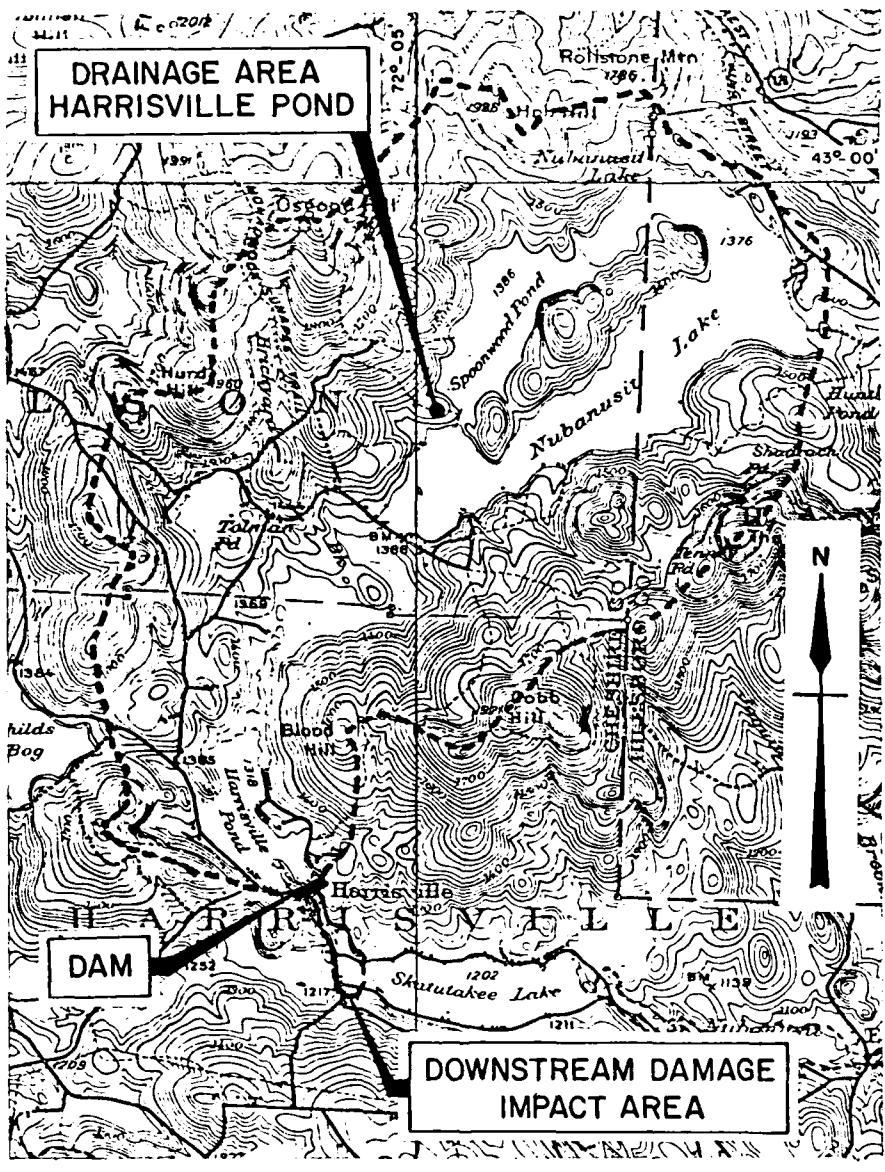
HARRISVILLE POND DAM

SCALE	1:250,000
DATE	APR 1967



### STORAGE CAPACITY - ELEVATION CURVE

FAY, SPOFFORD & THORNDIKE, INC. ENGINEERS BOSTON, MASS.	U.S. ARMY ENGINEER DIV. NEW ENGLAND CORPS OF ENGINEERS WALTHAM, MASS.
NATIONAL PROGRAM OF INSPECTION OF NON-FED. DAMS	
<b>HARRISVILLE POND DAM</b>	
NEW HAMPSHIRE	
SCALE	AS SHOWN
DATE	AUGUST, 1978



SCALE 1:62500 (ACTUAL)

UNITED STATES  
DEPARTMENT OF INTERIOR  
GEOLOGICAL SURVEY

NEW HAMPSHIRE  
MONADNOCK QUADRANGLE 1949  
AMS 6569 I-SERIES V712

LOVELL MOUNTAIN QUADRANGLE 1957  
AMS 6570 II-SERIES V712

APPENDIX E

INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS

# INVENTORY OF DAMS IN THE UNITED STATES

1 WATER NUMBER	2 WATER NUMBER	3 STATE	4 COUNTY OR DIST.	5 CITY OR TOWN	6 CONC. OR DIST.	7 NAME	8 LATITUDE (NORTH)	9 LONGITUDE (WEST)	10 REPORT DATE
65	65	NH	NH	HARRISVILLE POND		HARRISVILLE POND	42°56'7"	72°0'9"	15AUG70
(15)									
(16)									
(17)									
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